## ROOTSIMU V4.0

 A dynamic simulation of root growth, water uptake, and biomass partitioning in a soil-plant-atmosphere continuum: update and documentation

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## INTERPRETIVE SUMMARY

ROOTSIMU is a computer simulation model which describes the complex of interactions between the shoot and root systems of a crop growing vegetatively in a soil-plantatmosphere continuum. The model contains both a carbonbalance algorithm to account for many fundamental plant processes and a water-balance algorithm to account for water movement through both the plant and bulk soil. Maintenance of a functional balance between shoot and root size is facilitated by partitioning growth between new root and shoot tissue according to plant water potential. Readers are referred to Huck and Hillel (21) for additional, detailed discussions of the model logic. The model was originally developed on a mainframe computer, but versions are now available for miniand micro-computers.

## ROOTSIMU V4.0

# A Dynamic Simulation of Root Growth, Water Uptake, and Biomass Partitioning in a Soil-Plant-Atmosphere Continuum: Update and Documentation ${ }^{1}$ 

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## INTRODUCTION

AN EARLY VERSION of the model ROOTSIMU (version 1.5) has been described by Huck and Hillel (21). They explained their underlying assumptions and presented examples based on the use of a sine-function as the driver for the calculation of air and soil temperature and radiation intercepted by the canopy. The original version of the model permitted testing the plausibility of assumptions, but its predictions could not be tested against measured data because no provision for input of climatic data was included in the code. ROOTSIMU version 1.5 of the model was developed in Continuous System Modeling Program, an IBM computer simulation language referred to as CSMP3 $(24,36)$. CSMP contains integration and plotting subroutines and several other special functions and, therefore, it facilitates easy modifications and expansions of the source code.

A modification of the model is presented which permits the use of measured climatic data as driving functions. Arbitrary functions are generated by interpolation between known data points as described earlier (21). This new revision of the model (ROOTSIMU version 4.0) permits a comparison of predictions from the computer run under simulated conditions with experimentally determined data. The discrete daily input data, which are used to simulate the continuous weather conditions, are almost identical with those observed in actual experiments from which measurement data were obtained. However, the daily summation of each input variable is now adjusted to match observed values. Sections of the model which calculate photosynthesis and shoot and root growth also were revised.

The primary purpose of this publication is to incorporate the real weather capability into the model ROOTSIMU and to describe further modifications in other sections of the model. It includes a listing of the model ROOTSIMU version 4.0 in CSMP and FORTRAN and instructions to run the model on either a mainframe, mini-, or micro-computer.

Examples comparing predicted soybean root growth and water movement with actual experimental data from the 1981 growing season will be published by Hoogenboom et al. (17). Presented herein are some examples of soybean plant growth

[^0]data predicted by the simulation model for the 1983 growing season. Soybean (Glycine max [L.] Merr.) shoot and root growth as measured under experimental conditions during the 1983 growing season will be published elsewhere $(18,23)$. In the following examples, data recorded by a standard Class " A " weather station during the summer of 1983 (1) and summarized on a daily basis were used as a driver for the climate sections of the model.

## MODEL DESCRIPTION

The quantitative model ROOTSIMU, Appendix A-C, is a set of equations which describes the complex of interactions between the shoot and root systems of a crop growing vegetatively in a one dimensional soil profile, arbitrarily divided


FIG. 1. Hypothetical soybean plant growing in a one-dimensional layered soil consisting of uniform layers in the horizontal direction.
into discrete layers, figure $1(20)$. The model contains both carbon-balance and water-balance algorithms to describe such fundamental processes as photosynthesis, respiration, vegetative growth of shoot and root tissues (computed independently), transpiration and soil water uptake by roots, and water movement through bulk soil including effects of irrigation, rainfall, and drainage.

The carbon-balance section computes a photosynthetic rate per unit leaf area from regression-based temperature and photosynthetic active radiation (PAR) functions. Self-shading, when the leaf area index (LAI) is greater than 1, and stomatal closure, induced by low plant water potentials ( $\psi_{\text {plant }}$ ), reduce photosynthesis. Soluble carbohydrates derived from photosynthesis accumulate in a labile pool accessible to each organ. The soluble carbohydrates are withdrawn from this pool and are used in growth and respiratory processes at independently computed rates for each process. Maintenance respiration depends only on temperature and tissue mass, but growth respiration also depends upon the size of the reservecarbohydrate pool, figure 2. Shoot tissue necrosis is a function of leaf age and LAI, because at an LAI greater than 1 the lower leaves on the canopy are shaded by the upper leaves. Root death rate is a function of root age and carbohydrate reserve level. Maintenance of a functional balance between shoot and root size is facilitated by partitioning growth between new root and shoot tissue according to $\psi_{\text {plant }}$ (computed from tissue relative water content). As $\psi_{\text {plant }}$ plant declines with depletion of stored soil water reserves, root growth increases and shoot growth declines. Roots grow more rapidly


FIG. 2. Forrester flow diagram for carbon balance algorithm.


FIG. 3. Forrester flow diagram for water balance algorithm.
in wetter parts of the soil profile than in the drier parts of the soil profile, so younger roots with higher tissue conductivity form in wet soil, while older, non-functioning roots die in dry soil.

The water-balance section computes evaporative demand from incoming solar radiation and partitions water loss between transpiration and soil surface evaporation, according to LAI (soil shading) and hydraulic conductivity of the soil surface layer (a function of its water content). Internal water redistribution and sub-surface drainage are computed from $\psi$ gradients in bulk soil, while soil water uptake by roots is a catenary function of $\psi$ differences between leaves, root surface, and the water held in each soil layer, figure 3. A more detailed description of the basic logic of the carbon-balance and waterbalance section of the model is given by Huck and Hillel (21).

## MODEL MODIFICATIONS

The descriptions and code of the aboveground (shoot) portions of the model have been extensively revised to include recorded weather data for driving the model. Modules were taken from the published work of de Wit et al. (40) and Goudriaan and van Laar (11) and revised to fit this model, Appendix A. The automatic sort algorithm, which is a feature of CSMP, facilitated revisions to the CSMP simulation language source code (41). The UPDATE subroutine generated by the

CSMP translator was kept, modified, and stored as FORTRAN code.

This version of the model will run on a wide variety of mainframe, mini-, and micro-computers as an independent FORTRAN language program, Appendix B. Machinereadable copies of either source code are available from the authors on a 5.25 -inch diskette or by direct transmission electronic mail. An earlier version of the model (ROOTSIMU version 1.5) is available in Advanced Continuous Simulation Language identified as ACSL, Mitchell and Gauthier Assoc. (28), Appendix C. Basically, the simulation languages ACSL and CSMP are similar. However, in contrast to the simulation language CSMP which can only run on an IBM mainframe computer, the simulation language ACSL is available on a broader range of computers, including micro-computers. ${ }^{4}$

## Weather Data

In many applications when soil water relations and associated crop performance are simulated, the only long-term weather data available are those collected by a conventional meteorological observation station. Therefore, this model was written to include sections for interpolating between the discrete points (usually recorded at daily intervals) obtained from standard weather observations. The CSMP interpolation functions AFGEN and NLFGEN were used to generate continuous data between measured data points. A macro (macro is the equivalent of a subroutine) named WAVE, proposed by de Wit et al. (40), has been incorporated into the CSMP version of our model, Appendix A. This produces a continuous sine curve connecting maximum and minimum temperature values. Floyd and Braddock (8) reported that use of sine curve fitting can be an accurate way to model diurnal temperature curves. The FORTRAN version of the model, Appendix B, includes a homologous subroutine named WAVE which produces continuous-function output of the form required by the defining equations used in the model.

Interpolation schemes for solar radiation, rainfall (and/or irrigation events), open-pan evaporation, and air and soil temperature are included in the versions of the model illustrated here. Rainfall was assumed to infiltrate the surface at a constant rate over the full 24 -hour day when it was re-


FIG. 4. Simulated rate of instantaneous global radiation from day 230 to day 240, computed by WAVE algorithm.


FIG. 5. Simulated air (TEMP) and soil temperatures (STEMP) during days 230 to 240 . Both temperatures are calculated by forcing a sine function through the daily maximum air (MAXTEM) and soil temperatures and daily minimum air (MINTEM) and soil temperatures.
corded. The instantaneous potential evapotranspiration (ET) rate was interpolated from daily total pan evaporation measurements and proportioned according to the instantaneous radiation. Shaw and Laing (34) reported that, at full canopy, the evapotranspiration rate of soybeans is 90 percent of openpan evaporation. Similar observations were reported by Hanks (13) and Mason et al. (27). Alternative methods for computing ET rate, such as the energy-balance method of Penman (30), can be substituted by the user if adequate measurement data to support the desired computation method are available.

Length of the daily light period (LSNHS), height of the sun (SNHSS), and the time of sunrise (RISE) are computed each day from geometrical calculations based on latitude (LAT) and season (declination of the sun [DEC]). Daily totals for maximum and minimum solar radiation, for a completely clear day (DRC, DRCP) or for a completely overcast day (DRO, DROP), respectively, are estimated as a function of sun height, based on the assumptions of de Wit et al. (40). These computed daily solar radiation totals are then compared with the measured solar radiation (DTRR,DTR) observed for that day, and the ratios between measured radiation and that expected for a clear day or for an overcast day are computed (LFCL,LFOV). Finally, an instantaneous rate for solar radiation (RADIAT) is computed along a half-sine curve using the proportions of diffuse and clear-sky radiation computed earlier. The net effect of these computations defines a continuous function, figure 4 , which resembles figure 3 of Huck and Hillel (21) except that each day's total radiation is now adjusted to match that observed by the meteorological instrumentation.

Linear interpolation between successive daily minimum and maximum air temperatures (MINTMP,MAXTMP) provides a variable-width band, figure 5, within which WAVE generates a sinusoidal air temperature function with periodicity determined by the length of the daily light period. The same WAVE function is used to generate instantaneous soil temperatures between successive daily minimum and maximum soil temperatures (MNSTMP, MXSTMP). It is assumed that the daily minimum and maximum soil temperatures occur with a delay of 3 hours, compared to the minimum and
maximum air temperatures, and that the same soil temperature is observed throughout the whole soil profile.

## Carbon Balance

One of the principal changes from version 1.5 of the model is the inclusion of a section for predicting photosynthesis and plant growth patterned after the BACROS model of de Wit et al. (40) and presented in simplified form by Goudriaan and van Laar (11). The model ROOTSIMU computes two photosynthetic rates: PHOTC, the maximum canopy photosynthetic rate under a completely clear sky, and PHOTD, the maximum possible photosynthetic rate under a completely overcast sky. Adjustments for shading within the canopy (based upon LAI) are made according to the method described by Goudriaan and van Laar (11). Based on data reported by Shibles and Weber (35), it is assumed that 100 percent of the incoming radiation is intercepted by the soybean canopy if the LAI is larger than three. Respiration, assimilation, and growth are treated as in the earlier version 1.5 of this model.

Version 1.5 of this model (21) considered partitioning of carbohydrates only between the root system (ROOTW) and a shoot system (SHOOTW) consisting of a single compartment. The shoot system compartment has been expanded to include separate compartments for leaf (LEAFW) and for stem tissue (STEMW), which permits a more accurate representation of canopy architecture, figure 1 . It is assumed that stems only respire and that their photosynthetic capacity is small compared with the leaves, because of the relatively small surface area of the stems. It is assumed that the leaves, on the other hand, carry on both photosynthesis and respiration. Although it is known that the specific leaf area of soybean leaves varies with time and position (25), a constant specific leaf area is assumed in this model $(12,33)$.

Additional constraints have been imposed on root growth in the model. For instance, a maximum root density is imposed: the total volume of roots in any soil compartment can never exceed a set fraction of the total pore-space. This allows for incorporation of a plow layer and other factors which increase soil strength and cause a reduction in root growth (10). Taylor and Klepper (37) reported that the rooting volume depends on both species and environment. The volume of roots (ROOTVL) is computed from root mass (ROOTWT), diameter (LNGFAC), and density (PRTL). Soil porosity (POROS) also is computed for each layer, based on bulk density (BULKDS), which is a function of depth (DEPTH) and particle density (PARTDS).

It is further assumed that the propensity for new root growth (BIRTH) and extension of existing roots (EXTENS) is inversely proportional to depth, which takes into account the longitudinal resistance to carbohydrate and water transport in the phloem tissue. Vertical extension of roots into a new layer can only occur when root length in the other layer exceeds a minimum threshold, MINRTL. No root growth is permitted in the lowest soil layer, which is assumed to represent a buffer between the water table and the soil layers in which the roots are growing actively, figure 1. Because simulated root growth is highly responsive to soil moisture conditions, a soil layer which is saturated with water might show
an excessive amount of root growth, compared with the other drier soil layers. In the previous version (1.5) of the model, an unreasonably large mass of root tissue was predicted in the undrained bottom layer.

## Water Balance

Validation data were obtained from the experiments of Huck et al. $(22,23)$ in which soybean shoot and root growth was measured in the Auburn rhizotron under two different water regimes. The nonirrigated treatment (NI) was simulated by adding only the observed rainfall (RAIN) to the surface soil layer. In addition to observed rainfall, $250 \mathrm{~cm}^{3} \mathrm{~m}^{-3}$ of irrigation water (IRQUAN) was automatically (PULSSW) added to the simulated irrigated treatment (IR) every 30 minutes (PULSIR) whenever the computed soil water potential $\left(\psi_{\text {soil }}\right)$ at a depth of 0.4 m dropped below -15 kPa (IRMIN). In the rhizotron experiments, the trickle irrigation system was switched on for 3 to 5 minutes at hourly intervals whenever the tensiometer readings at a depth of 0.4 m fell below -10 to - 15 kpa (23). An example of the $\psi_{\text {sail }}$ measured by tensiometers at a depth of 0.4 m during the 1983 growing season is presented in figure 6.

The Darcian flow equations used to compute unsaturated water flow (NFLW) between layers has been retained in this version of the model, but infiltration is based on the assumptions of Green and Ampt (12). Water flows from the surface into deeper layers at a rate controlled by saturated conductivity (SATCON), but only when the matric potential of the conducting layer is near 0 . Since each increment of added water begins percolation in the surface layer, the FLPFLP (flipflop) function used in version 1.5 of the model (12) was eliminated. Each iterative calculation to balance water uptake by the roots, water flow in the soil and the plant, and transpiration now begins at the surface. When soil water content of any layer reaches saturation, flow through that layer is assumed to occur at the maximum (saturated conductivity) rate. Water is allowed to drain from the bottom layer to prevent accumulation in the soil profile (DRAING).

Relative conductivity was redefined as proposed by van Genuchten (38), and calculated as a function of soil matric potential. The constants ' $a$ ' (ALPHA) and ' $n$ ' (NU) were determined by nonlinear least-square analysis fit of the soil waterretention data (38). Possible vapor phase transport and the effects of entrapped air were ignored.

## MODEL INITIATION <br> Weather Data

Weather data used as drivers for the model included: daily total solar radiation (RADN; Watt hours day ${ }^{-1}$ or Joule day ${ }^{-1}$ ); daily minimum and maximum air temperatures (MINTEM, MAXTEM; degree Celsius or Fahrenheit); daily minimum and maximum soil temperatures (MINSTM, MAXSTM; degree Celsius or Fahrenheit); daily rainfall (CMRAIN; cm day ${ }^{-1}$ or inches day ${ }^{-1}$ ) and daily open pan evaporation (PEVAP cm day $^{-1}$ or inches day ${ }^{-1}$ ). Because the units in which weather data are recorded vary from weather station to weather station, the numbers must be converted into SI units for the model to function. Weather generators can be used if one or more input variables are missing. For instance, when no soil


FIG. 6. Soil water conditions for the 1983 growing season. Above: Measured soil water potential at a depth of 0.4 m during the 1983 growing season (tensiometer readings below - 50 kPa are subject to error). Below: Rainfall during the 1983 growing season and growth stages (6).
temperature data are available, it might be assumed that the soil temperature has a lag phase of 3 hours relative to air temperature.

The weather data used in demonstrating version 4.0 of the model were recorded during 1983 by the weather station at the Alabama Agricultural Experiment Station (1) located in Auburn. An example of the raw weather data for 1983 in the model is given in table 1. For calendar days 150 to 174 , the values shown represent, from left to right, in units as reported by the weather station, daily total radiation (Watt hours), daily maximum air temperature and daily minimum air temperature (Fahrenheit) measured at a height of 5 feet ( 1.5 m ) above the soil surface, daily total rainfall (inches), daily total open pan evaporation (inches), and daily maximum soil temperature and daily minimum soil temperature (Fahrenheit) measured at a depth of 4 inches ( 0.1 m ). The year and calendar day are given at the far right on each line. In the model, the units of the input variables are converted into SI-units.

## Plant Material

ROOTSIMU is a general root-growth model and can be used to simulate any type of plant, providing initiation variables and growth parameters are available. However, the input plant parameters used for this demonstration were chosen to match those of soybeans used for the validation data set collected at the Auburn rhizotron ( $18,19,22,23$ ). The starting day of the year (PARAM START $=150$ ), the number of simulation hours (FINISH HOURS $=2400$ hours), and the site of the crop (PARAM LAT $=32.5$ degree) were defined to match the actual crop grown. The initial shoot mass (PARAM ISHOOT $=0.010 \mathrm{~kg} \mathrm{~m}^{-2}$ ) was set to a value representing the mass of the first trifoliolate leaf as it was observed on day 150. A partitioning factor for weight distribution between the leaves and the stem (PARAM STWTR $=0.25$ ) and a specific leaf area parameter (PARAM LEAFTH $=30 \mathrm{~m}^{2} \mathrm{~kg}^{-1}$ ) were defined (33). For the roots, an initial root mass (PARAM

Table 1. Input Data File for Weather Data
From left to right, daily total solar radiation (RADN), daily maximum air temperature (MAXTEM), daily minimum air temperature (MINTEM), daily total rainfall (CMRAIN), daily total open pan evaporation (PEVAP), daily maximum soil temperature (MAXSTM), daily minimum soil temperature (MINSTM), year (YEAR), and calendar day (DAY)

| RADN MAXTEM |  | MINTEM | CMRAIN | $N$ PEVAP | MAXSTM | MINSTM | YEAR | DAY |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| W. hour | F | F | Inches | Inches | F | F |  |  |
| 5518 | 87.0 | 62.0 | 0.15 | 0.29 | 92 | 70 | 083 | 150 |
| 7397 | 88.0 | 62.0 | 0.00 | . 46 | 89 | 69 | 083 | 151 |
| 7377 | 83.0 | 59.0 | 0.00 | . 33 | 93 | 70 | 083 | 152 |
| 5666 | 78.0 | 53.0 | 0.00 | . 24 | 89 | 69 | 083 | 153 |
| 7700 | 83.0 | 60.0 | 0.00 | . 27 | 95 | 70 | 083 | 154 |
| 6943 | 88.0 | 64.0 | . 09 | . 30 | 96 | 74 | 083 | 155 |
| 5463 | 84.0 | 62.0 | 0.00 | . 20 | 92 | 75 | 083 | 156 |
| 4399 | 84.0 | 62.0 | 0.00 | . 16 | 91 | 75 | 083 | 157 |
| 5080 | 82.0 | 65.0 | . 48 | . 21 | 90 | 70 | 083 | 158 |
| 1511 | 72.0 | 58.0 | . 57 | . 09 | 76 | 68 | 083 | 159 |
| 7127 | 80.0 | 59.0 | 0.00 | . 26 | 86 | 68 | 083 | 160 |
| 6084 | 82.0 | 61.0 | 0.00 | . 23 | 86 | 68 | 083 | 161 |
| 7294 | 82.0 | 59.0 | 0.00 | . 31 | 89 | 68 | 083 | 162 |
| 7622 | 83.0 | 61.0 | 0.00 | . 33 | 92 | 70 | 083 | 163 |
| 7741 | 83.0 | 63.0 | 0.00 | . 38 | 94 | 71 | 083 | 164 |
| 7910 | 84.0 | 61.0 | 0.00 | . 37 | 97 | 73 | 083 | 165 |
| 6878 | 86.0 | 56.0 | 0.00 | . 26 | 97 | 73 | 083 | 166 |
| 6670 | 88.0 | 61.0 | 0.00 | . 26 | 97 | 74 | 083 | 167 |
| 5753 | 90.0 | 67.0 | 0.00 | . 17 | 98 | 76 | 083 | 168 |
| 4551 | 85.0 | 65.0 | . 23 | . 21 | 92 | 75 | 083 | 169 |
| 4108 | 83.0 | 65.0 | . 42 | . 24 | 87 | 73 | 083 | 170 |
| 2826 | 82.0 | 65.0 | . 47 | . 14 | 82 | 71 | 083 | 171 |
| 4944 | 82.0 | 67.0 | 0.00 | . 20 | 85 | 72 | 083 | 172 |
| 3218 | 79.0 | 67.0 | . 01 | . 14 | 81 | 73 | 083 | 173 |
| 4728 | 87.0 | 69.0 | . 02 | . 17 | 89 | 74 | 083 | 174 |

IROOT $=0.002 \mathrm{~kg} \mathrm{~m}^{-2}$ ), factors for root growth distribution over the top soil layers (TABLE RRL $(1-10)=0.54,0.38$, 0.08 , etc.), and root length to root mass ratio (PARAM LNGFAC $=13000 \mathrm{~m} \mathrm{~kg}^{-1}$ ) were determined from the experimental plants on day 150 .

The photosynthetic parameters are defined for $\mathrm{C}_{3}$-plants in general, but can be adjusted if necessary: maximum photosynthetic rate, PARAM MXPHOT $=0.82 * 10^{-6} \mathrm{~kg} \mathrm{~m}^{-2} \mathrm{~s}^{-1}$, $(39,11)$ a light efficiency factor of the photosynthesis process, PARAM EFF $=0.01388 * 10^{-6} \mathrm{~kg} \mathrm{~J}^{-1} \mathrm{~s}^{-1},(3,26,11)$; a maintenance respiration factor, PARAM RSPFAC $=1.0 * 10^{-7} \mathrm{kgkg}^{-1} \mathrm{~s}^{-1}$ $(31,32)$; a conversion efficiency factor, PARAM CONVRT $=$ $0.30 \mathrm{~kg} \mathrm{~kg}^{-1}(31,32)$, and a growth factor, PARAM GROFAC $=$ $1.0 * 10^{-5} \mathrm{~kg} \mathrm{~kg}^{-1} \mathrm{~s}^{-1}$, (40).

The model also includes an aging and senescence factor for shoot tissue (PARAM AGFAC) which was set at $3.0 * 10^{-7}$ $\mathrm{kg} \mathrm{kg}^{-1} \mathrm{~s}^{-1}$ and a death factor for root tissue (PARAM

DTHFAC) which was set at $1.0 * 10^{-8} \mathrm{~kg} \mathrm{~kg}^{-1} \mathrm{~s}^{-1}$. Both of these gave a good fit to the experimental data, although shoot and root death rates were not actually measured.
FRAC is a factor which partitions dry matter between the shoot and the roots, based on canopy water potential. The function FRACTB, which is used to compute an instantaneous value for FRAC, was redefined. Similarly, the function LAIFAC, which is the basis for computing photosynthetic rate from LAI and partitions water loss between the canopy and the soil, was redefined. Both functions can be adjusted when data are available. The water stress table (FUNCTION TRNTBL) was adapted from data for soybean plants (5), but the data in the table can be substituted with other values for different crops.
Root growth was divided into root branching, which was the formation of new roots and the extension of older roots in the same soil layer, and root extension which was the exten-

Table 2. Input Data File for Plant and Soil Parameters (Corresponding to READ Statement in FORTRAN Program)

sion of root from one layer into the next layer. A relative branching factor (PARAM BR) was set at $1.0 * 10^{-4} \mathrm{~m} \mathrm{~s}^{-1}$ and the minimum $\psi_{\text {soil }}$ at which root branching terminates (PARAM BRMIN) was defined as -10 kPa . A relative extension factor (PARAM EXTNRT) was set at $3.0 * 10^{-3} \mathrm{~m} \mathrm{~s}^{-1}$ and a minimum $\psi_{\text {soil }}$ at which root extension from one layer into the next layer terminates (PARAM EXTMIN) was defined as -20 kPa . A factor to reduce root growth at increasing depth (PARAM DEPTHG) was set to $10 \mathrm{~m} \mathrm{~m}^{-1}$.

Although measured root water uptake is more closely related to total root surface area (7), in this model, root resistance and water uptake rates are based on root length, which assumes a linear relationship between root length and root surface area (7). For root water uptake, an axial resistance (PARAM UARS $=1.0 * 10^{11} \mathrm{~s} \mathrm{~m} \mathrm{~m} \mathrm{~m}^{-1}$ ), a radial resistance $\left(\right.$ PARAM URRS $\left.=1.0 * 10^{11} \mathrm{~s} \mathrm{~m}\right)$, and a factor relating soil conductivity, root length, and root conductivity, PARAM B = $0.01 \mathrm{~m}^{-1}(9)$ are required. The input parameters needed to define the initial plant conditions are shown in table 2, which is set up in the format to be read by the FORTRAN program in Appendix B and can be adjusted by the user. For instance, the first line in table 2 shows, respectively, the finished condition in seconds for the simulation run (FINTIM), the output intervals for plotting (OUTDEL) or printing (PRDEL), the time step of each simulation interval (DELT), and finally the starting day of the simulation run (BGNDAY).

## Soil Conditions

Soil conditions are an important part of the model and greatly influence the results of the simulation. The experimental plants were grown in the A-horizon from a Dothan loamy sand (fine loamy, siliceous, thermic Plinthic Paleudult). A soil-water retention curve for this soil material was experimentally measured in the laboratory and used as a basis for defining the function SUTB. Saturated water content (PARAM STHETA $=0.36 \mathrm{~m}^{3} \mathrm{~m}^{-3}$ ), air dry water content (PARAM THTAIR $=0.050 \mathrm{~m}^{3} \mathrm{~m}^{-3}$ ), bulk density as a function of depth (FUNCTION BULKF), and particle density (PARAM PARTDS $=2.59 \mathrm{Mg} \mathrm{m}^{-3}$ ) were also measured in the laboratory and used as input parameters in the model (4). To calculate water flow, a saturated conductivity (PARAM SATCON $=5.0 * 10^{-5} \mathrm{~m}_{\text {day }}{ }^{-1}$ ) and the constants to define the van Genuchten (38) equation for calculating relative conductivity must be defined (PARAM ALPHA $=0.24890$; PARAM $\mathrm{NU}=1.21555$ ).

In this revision of the model, the homogeneous soil profile was arbitrarily divided into 10 layers (PARAM NJ $=10$ ) of $0.20 \mathrm{~m}\left(\operatorname{TABLE} \operatorname{TCOM}(1-20)=0.10,2^{*} 0.15,17^{*} 0.20 \mathrm{~m}\right)$ except for the three top layers, which were $0.10,0.15$, and 0.15 m , respectively. The thickness of each layer can easily be adjusted if necessary.

The model provides an option for simulating irrigation treatments. A minimum $\psi_{\text {soil }}$ threshold matching the tensiometer readings (PARAM IRFAC $=10 \mathrm{kPa}$ ) and the amount applied per irrigation pulse (PARAM IRQUAN $=(0.0,250.0$ $\mathrm{cm}^{3} \mathrm{~m}^{-2}$ ) were defined.

Most of the initial soil conditions are shown in table 2, which represents an input file read on device \#8 for the FORTRAN version (Appendix B) of the model. When the CSMP version of the model is used, both the IR and NI treat-
ments can be run simultaneously and the results can be overlayed on plots.

## MODEL RESTRICTIONS

One of the main limitations of this revision of the model is that it has no provisions for partitioning dry matter into reproductive structures such as flowers, pods, or seeds. Because Braxton (maturity group VII) soybean plants continue vigorous vegetative growth throughout the full-bloom (R2) and beginning pod-set (R3) stages (6), this portion of the growing season was included in the simulation examples presented below. When plants began full pod development (R4) and early-seed-filling stages (R5), most of the available dry matter was stored in pods and seeds. Thus, this version of the model, which accounts for vegetative growth only, cannot adequately describe carbon partitioning during seed formation and maturation. Therefore, only the first 100 days of the growing season, during which most of the vegetative soybean growth occurs, were simulated.

Because the model was developed mainly to simulate the effect of water stress on plant growth, it was assumed that the supply of nutrients would be optimal and that growth would not be inhibited by insects, diseases, or weeds. The model also did not account for soil environmental constraints (21), such as poor aeration, temperature extremes, salinity, or chemical toxicity, although they could be included if data were available. Some of these simplifications and assumptions of the model will be replaced by newly coded algorithms as the model is extended.

## MODEL PREDICTIONS

Only predictions for the 1983 growing season are presented herein. Detailed trial simulation runs for the 1981 growing season, including comparisons between observed and simulated data, are described by Hoogenboom et al. (17).

## Environmental Conditions

Figure 4 shows the intensity of solar radiation expressed as a continuous function over a 10-day period of the growing sea-

CALENDAR DAY


FIG. 7. Simulated water potential (POTM(4)) at a depth of 0.4 m from day 150 to day 250.
son as interpolated by the computer from measured daily totals. Soil and ambient-air temperature over the same 10 -day period are shown in figure 5 (TEMP, STEMP), including the daily maximum (MAXTEM) and minimum (MINTEM) air temperature. Rainfall events as measured at the Auburn rhizotron are presented in figure 6. This figure also presents the experimentally measured $\psi_{\text {soil }}$ for the 1983 growing season, while the simulated $\psi_{\text {soil }}$ is shown in figure 7 . The data for ex-. perimental and simulated NI treatments show low $\psi_{\text {soil }}$ during the period without rainfall from day 205 to 215 and from day 225 to 250 . Detailed model predictions from day 230 to 240 are presented in the next simulation examples, because during this period strong differences between IR and NI plants were observed.

## Plant Growth

Because little rain was observed between days 230 and 240 , figure 6 b , canopy water potential ( $\psi_{\text {canopy }}$ ) of the simulated NI plants reached lower values than $\psi_{\text {canopy }}$ of simulated IR plants as the drought period continued, figure 8. Although simulated $\psi_{\text {canopy }}$ and therefore water stress levels were different with the two treatments, no differences were observed between simulated photosynthetic rates, figure 9 . The lower $\psi_{\text {canopy }}$ of the simulated NI plants induced an increasing pro-

CALENDAR DAY


FIG. 8. Simulated canopy water potential (POTCR) from day 230 to day 240.


FIG. 9. Simulated canopy apparent photosynthesis (PHOTSN) from day 230 to day 240 .


FIG. 10. Simulated partitioning factor for dry matter (FRAC) from day 230 to day 240.
portion of the available dry matter to be used by the roots, as shown by the partitioning factor FRAC, figure 10 . Although predicted shoot growth of both treatments was similar during this period, figure 11A, predicted root growth, especially in the NI plants, increased markedly, figure 12A. Predicted shoot death rates, figure 11 B , increased during this period, while predicted root death rates had similar maximum rates every day, figure 12B.

Long term growth of shoot and root mass as predicted by


FIG. 11. Simulated growth and death rates of the shoot system from day 230 to day 240. A: Growth rates (TOPGRO). B: Death rates (SHOOTD)


FIG. 12. Simulated growth and death rates of the root system from day 230 to day 240. A: Growth rates (TOTRG). B: Death rates (ROOTDY).
the model is presented in figure 13. Although there was no difference in simulated total dry weight of the two treatments, simulated IR plants had a larger shoot and therefore more leaf area, figure 14 . On the other hand, simulated NI plants had a heavier root system with larger total root length, figure 15. The difference between the predicted root lengths of the two treatments was mainly found in the deeper soil layers, figure 16D, similar to experimental observations $(18,19)$. No root growth was predicted in the surface layer for either treatment, figure 16A. Most of the predicted root growth was found between a depth of 0.25 and 1.00 m , figure 16 B and C. The simulated IR plants had a larger root system between a depth of 0.60 and 1.00 m , while simulated NI plants had a larger root system between 1.00 and 1.40 m , figure 16C and D.

During the drought period between days 230 and 240, figure 6, a decrease in simulated net root growth occurred above 0.40 m , figure 17A, in the NI treatment. Simulated IR plants formed roots mainly between 0.25 and 0.80 m , while simulated NI plants formed roots mainly between 0.80 and 1.40 m , figure 17. The model predicted no water extraction from the top layer, because it was extremely dry due to evaporation. It therefore contained only the tap root and no small feeder roots, figure 17A. Simulated IR plants mainly extracted water between 0.25 m and 0.80 m , figure 17A and B, while NI plants mainly extracted water between 0.80 and 1.20 m , figure 17 C and D. Predicted water extraction pat-


FIG. 13. Simulated dry matter accumulation in the whole plant (DRYWT), the shoot system (SHOOTW), and the root system (ROOTW) from day 150 to day 250.


FIG. 14. Simulated increase in leaf area index (LAI) from day 150 to day 250.


FIG. 15. Simulated increase in total root length (ROOTL) from day 150 to day 250 .


FIG. 16. Simulated root growth from day 150 to day 250. A: Between $0.00-0.10 \mathrm{~m}$ and between $0.10-0.25 \mathrm{~m}$. B: Between 0.25-0.40 m and between 0.40-0.60 m. C: Between 0.60-0.80 m and between 0.80-1.00 m. D: Between 1.00-1.20 mand between 1.20-1.40 m.


FIG. 17. Simulated net change in root length between day 230 and 240. A : Between 0.00-0.10 mand between 0.10-0.25 m. B: Between 0.250.40 m and between $0.40-0.60 \mathrm{~m}$. C: Between $0.60-0.80 \mathrm{~m}$ and between $0.80-1.00 \mathrm{~m}$. D: Between 1.00-1.20 m and between 1.20-1.40 m.


FIG. 18. Simulated soil water uptake between day 230 and day 240. A: Between $0.00-0.10 \mathrm{~m}$ and between $0.10-0.25 \mathrm{~m}$. B: Between 0.25-0.40 m and between 0.40-0.60 m. C: Between 0.60-0.80 mand between 0.80-1.00 m. D: Between 1.00-1.20 m and between 1.20-1.40 m.
terns, figure 17, were similar to predicted root growth patterns by the simulation model, figure 18 .

These examples show some of the capabilities of the model ROOTSIMU, version 4.0. Other variables, which represent either an environmental or plant parameter, are involved in the simulation process. The list of variables included in the model is given in Appendix D.

## SIMULATION INSTRUCTIONS

The examples illustrated herein were generated by the CSMP version of the model. The UPDATE subroutine generated by the CSMP translator was kept and stored on disk on a mainframe computer so that the model could be run independently. The FORTRAN version of the model has been adapted and tested, so that results from this version of the model are the same as those obtained by running the CSMP version.

## Mainframe or Mini-Computer

If a CSMP-package is available on a larger mainframe or mini-computer, the program can be run in a background mode, using the proper job control language and weather file as input data set, table 1. Plant and soil parameters are included in the CSMP version of the model. Because CSMP has a built-in plotting routine, output data sets need not be explicitly defined, and results will be plotted as specified on
the XYPLOT statements. A similar strategy is applicable if an ACSL package is available (28).
If no simulation languages are available, the FORTRAN version of the model can also be run on any larger mainframe computer with a FORTRAN compiler. This FORTRAN version is less dynamic and subroutines must be included for many of the calculations which are performed automatically by CSMP or ACSL. The FORTRAN version of the model generally can be run in a background mode, while specifying UNIT 8 as input for the plant and soil parameters, table 2, and UNIT 12 as input for the weather data, table 1. Other device addresses can be specified as output files. After completion of the simulation, the output files are saved and then used for plotting with X-Y plotting routines adapted to the computer system available. An example of an output file is presented in table 3. Shown are rates of photosynthesis (PHOTSN), respiration (RESP), growth (GROWTH), transpiration (TRANSP), evaporation (EVAP), and water uptake from all soil layers (SUMR) on an hourly (HOURS) basis for the first 24 hours of simulation, starting on day 150 .

## Micro-Computer

The following instructions to run the FORTRAN version of the model on a micro-computer apply only for an $\mathrm{IBM}^{3}-\mathrm{PC}$ or compatible computer. The FORTRAN source code of Appendix B is compiled, linked, and stored in a binary field named

Table 3. Output Data Files on Disk
From left to right, hours of simulation (HOURS), photosynthetic rate (PHOTSN), growth rate (GROWTH), respiration rate (RESP), total water uptake by the roots (SUMR), evaporation rate (EVAP), and transpiration rate (TRANSP).

| HOURS 1 | PHOTSN | GROWTH | RESP | SUMR | EVAP | TRANSP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| h | $\mathrm{kg} \mathrm{m}-2 \mathrm{~s}-1$ | $\mathrm{~kg} \mathrm{~m}-2 \mathrm{~s}-1$ | $\mathrm{~kg} \mathrm{~m}-2 \mathrm{~s}-1$ | $\mathrm{~m} \mathrm{~s}-1$ | $\mathrm{~m} \mathrm{~s}-1$ | $\mathrm{~m} \mathrm{~s}-1$ |
| $0.000 \mathrm{E}+00$ | $0.754 \mathrm{E}-18$ | $0.279 \mathrm{E}-08$ | $0.934 \mathrm{E}-09$ | $0.228 \mathrm{E}-09$ | $0.805 \mathrm{E}-09$ | $0.480 \mathrm{E}-10$ |
| $.100 \mathrm{E}+01$ | $.754 \mathrm{E}-18$ | $.241 \mathrm{E}-08$ | $.162 \mathrm{E}-08$ | $.235 \mathrm{E}-09$ | $.824 \mathrm{E}-09$ | $.492 \mathrm{E}-10$ |
| $.200 \mathrm{E}+01$ | $.754 \mathrm{E}-18$ | $.214 \mathrm{E}-08$ | $.146 \mathrm{E}-08$ | $.242 \mathrm{E}-09$ | $.844 \mathrm{E}-09$ | $.504 \mathrm{E}-10$ |
| $.300 \mathrm{E}+01$ | $.754 \mathrm{E}-18$ | $.195 \mathrm{E}-08$ | $.135 \mathrm{E}-08$ | $.248 \mathrm{E}-09$ | $.863 \mathrm{E}-09$ | $.516 \mathrm{E}-10$ |
| $.400 \mathrm{E}+01$ | $.754 \mathrm{E}-18$ | $.184 \mathrm{E}-08$ | $.129 \mathrm{E}-08$ | $.254 \mathrm{E}-09$ | $.883 \mathrm{E}-09$ | $.528 \mathrm{E}-10$ |
| $.500 \mathrm{E}+01$ | $.754 \mathrm{E}-18$ | $.178 \mathrm{E}-08$ | $.126 \mathrm{E}-08$ | $.255 \mathrm{E}-09$ | $.903 \mathrm{E}-09$ | $.540 \mathrm{E}-10$ |
| $.600 \mathrm{E}+01$ | $.173 \mathrm{E}-07$ | $.197 \mathrm{E}-08$ | $.128 \mathrm{E}-08$ | $.218 \mathrm{E}-08$ | $.368 \mathrm{E}-07$ | $.220 \mathrm{E}-08$ |
| $.700 \mathrm{E}+01$ | $.214 \mathrm{E}-07$ | $.243 \mathrm{E}-08$ | $.145 \mathrm{E}-08$ | $.486 \mathrm{E}-08$ | $.826 \mathrm{E}-07$ | $.495 \mathrm{E}-08$ |
| $.800 \mathrm{E}+01$ | $.231 \mathrm{E}-07$ | $.304 \mathrm{E}-08$ | $.171 \mathrm{E}-08$ | $.748 \mathrm{E}-08$ | $.128 \mathrm{E}-06$ | $.767 \mathrm{E}-08$ |
| $.900 \mathrm{E}+01$ | $.238 \mathrm{E}-07$ | $.377 \mathrm{E}-08$ | $.206 \mathrm{E}-08$ | $.967 \mathrm{E}-08$ | $.167 \mathrm{E}-06$ | $.999 \mathrm{E}-08$ |
| $.100 \mathrm{E}+02$ | $.242 \mathrm{E}-07$ | $.457 \mathrm{E}-08$ | $.246 \mathrm{E}-08$ | $.113 \mathrm{E}-07$ | $.197 \mathrm{E}-06$ | $.118 \mathrm{E}-07$ |
| $.110 \mathrm{E}+02$ | $.243 \mathrm{E}-07$ | $.546 \mathrm{E}-08$ | $.291 \mathrm{E}-08$ | $.124 \mathrm{E}-07$ | $.215 \mathrm{E}-06$ | $.129 \mathrm{E}-07$ |
| $.130 \mathrm{E}+02$ | $.243 \mathrm{E}-07$ | $.635 \mathrm{E}-08$ | $.335 \mathrm{E}-08$ | $.126 \mathrm{E}-07$ | $.220 \mathrm{E}-06$ | $.133 \mathrm{E}-07$ |
| $.130 \mathrm{E}+02$ | $.242 \mathrm{E}-07$ | $.718 \mathrm{E}-08$ | $.373 \mathrm{E}-08$ | $.123 \mathrm{E}-07$ | $.215 \mathrm{E}-06$ | $.130 \mathrm{E}-07$ |
| $.140 \mathrm{E}+02$ | $.240 \mathrm{E}-07$ | $.789 \mathrm{E}-08$ | $.400 \mathrm{E}-08$ | $.115 \mathrm{E}-07$ | $.197 \mathrm{E}-06$ | $.119 \mathrm{E}-07$ |
| $.150 \mathrm{E}+02$ | $.237 \mathrm{E}-07$ | $.859 \mathrm{E}-08$ | $.424 \mathrm{E}-08$ | $.975 \mathrm{E}-08$ | $.167 \mathrm{E}-06$ | $.101 \mathrm{E}-07$ |
| $.160 \mathrm{E}+02$ | $.229 \mathrm{E}-07$ | $.909 \mathrm{E}-08$ | $.442 \mathrm{E}-08$ | $.753 \mathrm{E}-08$ | $.128 \mathrm{E}-06$ | $.776 \mathrm{E}-08$ |
| $.170 \mathrm{E}+02$ | $.214 \mathrm{E}-07$ | $.919 \mathrm{E}-08$ | $.449 \mathrm{E}-08$ | $.491 \mathrm{E}-08$ | $.826 \mathrm{E}-07$ | $.502 \mathrm{E}-08$ |
| $.180 \mathrm{E}+02$ | $.175 \mathrm{E}-07$ | $.895 \mathrm{E}-08$ | $.439 \mathrm{E}-08$ | $.223 \mathrm{E}-08$ | $.369 \mathrm{E}-07$ | $.225 \mathrm{E}-08$ |
| $.190 \mathrm{E}+02$ | $.751 \mathrm{E}-18$ | $.801 \mathrm{E}-08$ | $.413 \mathrm{E}-08$ | $.104 \mathrm{E}-09$ | $.118 \mathrm{E}-08$ | $.717 \mathrm{E}-10$ |
| $.200 \mathrm{E}+02$ | $.754 \mathrm{E}-18$ | $.687 \mathrm{E}-08$ | $.367 \mathrm{E}-08$ | $.108 \mathrm{E}-09$ | $.120 \mathrm{E}-08$ | $.730 \mathrm{E}-10$ |
| $.210 \mathrm{E}+02$ | $.754 \mathrm{E}-18$ | $.581 \mathrm{E}-08$ | $.322 \mathrm{E}-08$ | $.113 \mathrm{E}-09$ | $.122 \mathrm{E}-08$ | $.743 \mathrm{E}-10$ |
| $.220 \mathrm{E}+02$ | $.754 \mathrm{E}-18$ | $.490 \mathrm{E}-08$ | $.281 \mathrm{E}-08$ | $.118 \mathrm{E}-09$ | $.124 \mathrm{E}-08$ | $.756 \mathrm{E}-10$ |
| $.230 \mathrm{E}+02$ | $.754 \mathrm{E}-18$ | $.416 \mathrm{E}-08$ | $.246 \mathrm{E}-08$ | $.125 \mathrm{E}-09$ | $.125 \mathrm{E}-08$ | $.768 \mathrm{E}-10$ |
| $.240 \mathrm{E}+02$ | $.391 \mathrm{E}-18$ | $.355 \mathrm{E}-08$ | $.216 \mathrm{E}-08$ | $.129 \mathrm{E}-09$ | $.127 \mathrm{E}-08$ | $.781 \mathrm{E}-10$ |

$1_{\text {Definition }}$ and unit for each variable are given in Appendix $D$.

ROOTSIMU.EXE. To run this FORTRAN-compiled version of the model simply type:

## ROOTSIMU

The program will respond with:
File name missing or blank
Please enter name : UNIT8?
Then type:
INPUTSG.FIL (inputs as in table 2)
to read the plant and soil parameters, presented in table 2.
UNIT12?
Then type:
DAT 1983.FIL (inputs as in table 1)
to read the weather data, presented in table 1.
UNIT6?
Then type:
CON for console (display or keyboard) or
LPT1 or PRN for printer.

The program will now start reading the data and weather files and will print the first line of the weather data set
 followed by:

## INITIATE

and the input weather data as presented for the first 25 days in table 4. After the program has read the last data line, it will come back and ask for an output file name

UNIT1?
Then type:
B:OUTPUT.FIL assuming a 2-drive machine; use
C:OUTPUT.FIL if hard disk is available.
The program will inform the user that it has finished the input and initiation process:

INITIATION NOW COMPLETE. ENTER DYNAMIC LOOP
and will write the results of the simulation at the fixed time

Table 4. Output Data Sent to Screen or Printer During Initiation of the Model

From left to right, calendar day (SIMDAY), daily total solar radiation (RADN), daily maximum air temperature (MAXTEM), daily minimum air temperature (MINTEM), daily total rainfall (CMRAIN), daily total open pan evaporation (PEVAP), daily maximum soil temperature (MAXSTM), daily minimum soil temperature (MINSTM), month (MONTH), and day of the month (DATE)

| SIMDAY 1 | RADN | MAXTEM | MINTEM | CMRAIN | PEVAP | MAXSTM | MINSTM | MONTH | DATE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| day | J m-2 | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{C}$ | $m$ day-1 | m day- | $-1{ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{C}$ |  |  |
| 150.0 | $0.20 \mathrm{E}+08$ | 30.56 | 16.67 | 0.38 | 0.74 | 33.33 | 21.11 | 5 | 30 |
| 151.0 | . $27 \mathrm{E}+08$ | 31.11 | 16.67 | 0.00 | 1.17 | 31.67 | 20.56 | 5 | 31 |
| 152.0 | . $27 \mathrm{E}+08$ | 28.33 | 15.00 | 0.00 | . 84 | 33.89 | 21.11 | 6 | 1 |
| 153.0 | .20E+08 | 25.56 | 11.67 | 0.00 | . 61 | 31.67 | 20.56 | 6 | 2 |
| 154.0 | . $28 \mathrm{E}+08$ | 28.33 | 15.56 | 0.00 | . 69 | 35.00 | 21.11 | 6 | 3 |
| 155.0 | . $25 \mathrm{E}+08$ | 31.11 | 17.78 | . 23 | . 76 | 35.56 | 23.33 | 6 | 4 |
| 156.0 | . $20 \mathrm{E}+08$ | 28.89 | 16.67 | 0.00 | . 51 | 33.33 | 23.89 | 6 | 5 |
| 157.0 | . $16 \mathrm{E}+08$ | 28.89 | 16.67 | 0.00 | . 41 | 32.78 | 23.89 | 6 | 6 |
| 158.0 | .18E+08 | 27.78 | 18.33 | 1.22 | . 53 | 32.22 | 21.11 | 6 | 7 |
| 159.0 | . $54 \mathrm{E}+07$ | 22.22 | 14.44 | 1.45 | . 23 | 24.44 | 20.00 | 6 | 8 |
| 160.0 | . $26 \mathrm{E}+08$ | 26.67 | 15.00 | 0.00 | . 66 | 30.00 | 20.00 | 6 | 9 |
| 161.0 | . $22 \mathrm{E}+08$ | 27.78 | 16.11 | 0.00 | . 58 | 30.00 | 20.00 | 6 | 10 |
| 162.0 | . $26 \mathrm{E}+08$ | 27.78 | 15.00 | 0.00 | . 79 | 31.67 | 20.00 | 6 | 11 |
| 163.0 | . $27 \mathrm{E}+08$ | 28.33 | 16.11 | 0.00 | . 84 | 33.33 | 21.11 | 6 | 12 |
| 164.0 | . $28 \mathrm{E}+08$ | 28.33 | 17.22 | 0.00 | . 97 | 34.44 | 21.67 | 6 | 13 |
| 165.0 | . $28 \mathrm{E}+08$ | 28.89 | 16.11 | 0.00 | . 94 | 36.11 | 22.78 | 6 | 14 |
| 166.0 | . $25 \mathrm{E}+08$ | 30.00 | 13.33 | 0.00 | . 66 | 36.11 | 22.78 | 6 | 15 |
| 167.0 | . $24 \mathrm{E}+08$ | 31.11 | 16.11 | 0.00 | . 66 | 36.11 | 23.33 | 6 | 16 |
| 168.0 | . $21 \mathrm{E}+08$ | 32.22 | 19.44 | 0.00 | . 43 | 36.67 | 24.44 | 6 | 17 |
| 169.0 | . $16 \mathrm{E}+08$ | 29.44 | 18.33 | . 58 | . 53 | 33.33 | 23.89 | 6 | 18 |
| 170.0 | . $15 \mathrm{E}+08$ | 28.33 | 18.33 | 1.07 | . 61 | 30.56 | 22.78 | 6 | 19 |
| 171.0 | .10E+08 | 27.78 | 18.33 | 1.19 | . 36 | 27.78 | 21.67 | 6 | 20 |
| 172.0 | . $18 \mathrm{E}+08$ | 27.78 | 19.44 | 0.00 | . 51 | 29.44 | 22.22 | 6 | 21 |
| 173.0 | . $12 \mathrm{E}+08$ | 26.11 | 19.44 | . 03 | . 36 | 27.22 | 22.78 | 6 | 22 |
| 174.0 | . $17 \mathrm{E}+08$ | 30.56 | 20.56 | . 05 | . 43 | 31.67 | 23.33 | 6 | 23 |
| 175.0 | .10E+08 | 25.56 | 18.33 | . 03 | . 33 | 27.78 | 22.22 | 6 | 24 |

$1_{\text {Definition }}$ and unit for each variable are given in Appendix $D$.
step interval read from unit 8 into this output file. For every hour of simulation it will also print the information presented in table 5 on the screen, to keep the user up to date with the progress of the current simulation run. The output file, table 3 , can be read after the simulation is finished, and can be split into different data sets according to the output specification. These data sets can then be plotted by the X-Y plotting routines, available on the micro-computer.
Without an 8087 coprocessor, it takes about 14 seconds to simulate 1 hour of plant growth on an IBM-PC ${ }^{3}$. To speed up the simulation process, longer time steps can be used or less
output can be generated. Another option is to use different math coprocessors or another micro-computer.

## DISCUSSION

An update of the model ROOTSIMU version 4.0 described by Huck and Hillel (21) is presented. The major changes made in the model are inclusion of input statements, which read daily observed climatic data, and algorithms which calculate instantaneous values from given daily totals. The shoot was divided into a stem part and a leaf part and a new canopy-

Table 5. Output Data Sent to Screen or Printer During Current Simulation Run

From left to right, calendar day (JULIAN), shoot dry matter (SHOOTW), root dry matter (ROOTW), leaf area index (LAI), root length (ROOTL), photosynthetic rate (PHOTSN), canopy water potential (POTCR), and transpiration rate (TRANSP)

JULIAN $=150.00$ SHOOTW $=0.01000$ ROOTW $=\quad 0.00200$ LAI $=0.225$

ROOTL $=\quad 26.009$ PHOTSN $=$| $0.75 E-18 ~ P O T C R ~$ |
| ---: | :--- |$\quad-2.00$ TRANSP $=0.48 E-10$

JULIAN $=150.04$ SHOOTW $=0.01001$ ROOTW $=0.00200$ LAI 0.225 ROOTL $=25.993$ PHOTSN $=0.75 \mathrm{E}-18$ POTCR $=\quad-2.00$ TRANSP $=0.49 \mathrm{E}-10$

JULIAN $=150.08$ SHOOTW $=0.01002$ ROOTW $=0.00200$ LAI $=0.225$
ROOTL $=25.976$ PHOTSN $=0.75 \mathrm{E}-18$ POTCR $=\quad-2.00$ TRANSP $=0.50 \mathrm{E}-10$
JULIAN $=150.12$ SHOOTW $=0.01002$ ROOTW $=0.00200$ LAI $=0.225$ ROOTL $=25.959$ PHOTSN $=0.75 \mathrm{E}-18$ POTCR $=\quad-2.00$ TRANSP $=0.52 \mathrm{E}-10$

JULIAN $=150.17$ SHOOTW $=0.01003$ ROOTW $=0.00200$ LAI $=0.226$ ROOTL $=25.941$ PHOTSN $=0.75 \mathrm{E}-18$ POTCR $=\quad-2.00$ TRANSP $=0.53 \mathrm{E}-10$

JULIAN $=150.21$ SHOOTW $=0.01004$ ROOTW $=0.00199$ LAI $=0.226$ ROOTL $=25.923$ $\operatorname{PHOTSN}=0.75 \mathrm{E}-18$ POTCR $=\quad-2.00$ TRANSP $=0.54 \mathrm{E}-10$

JULIAN $=150.25$ SHOOTW $=0.01004$ ROOTW $=0.00199$ LAI $=0.226$ ROOTL $=25.906$ $\operatorname{PHOTSN}=0.17 \mathrm{E}-07$ POTCR $=\quad-12.70$ TRANSP $=0.22 \mathrm{E}-08$

JULIAN $=150.29$ SHOOTW $=0.01005$ ROOTW $=0.00199$ LAI $=0.226$
ROOTL $=25.901$ PHOTSN $=0.21 \mathrm{E}-07$ POTCR $=\quad-27.69$ TRANSP $=0.49 \mathrm{E}-08$
JULIAN $=150.33$ SHOOTW $=0.01006$ ROOTW $=0.00199$ LAI $=0.226$
ROOTL $=25.912$ PHOTSN $=0.23 \mathrm{E}-07$ POTCR $=-42.57$ TRANSP $=0.76 \mathrm{E}-08$
JULIAN $=150.37$ SHOOTW $=0.01007$ ROOTW $=0.00200$ LAI $=0.226$
ROOTL $=25.943$ $\operatorname{PHOTSN}=0.24 \mathrm{E}-07$ POTCR $=\quad-57.11$ TRANSP $=0.98 \mathrm{E}-08$
JULIAN $=150.42$ SHOOTW $=0.01008$ ROOTW $=0.00200$ LAI $=0.227$
ROOTL $=25.989$ PHOTSN $=0.24 \mathrm{E}-07$ POTCR $=\quad-71.17$ TRANSP $=0.11 \mathrm{E}-07$
JULIAN $=150.46$ SHOOTW $=0.01009$ ROOTW $=0.00200$ LAI $=0.227$
ROOTL $=26.053$ $\operatorname{PHOTSN}=0.24 \mathrm{E}-07$ POTCR $=\quad-83.54$ TRANSP $=0.12 \mathrm{E}-07$
JULIAN $=150.50$ SHOOTW $=0.01010$ ROOTW $=0.00201$ LAI $=0.227$
ROOTL $=26.137$ $\operatorname{PHOTSN}=0.24 \mathrm{E}-07$ POTCR $=\quad-92.39$ TRANSP $=0.13 \mathrm{E}-07$

[^1]photosynthesis section was added. The root-growth and water-uptake sections were further refined and a section which reduces root growth under severe soil impedance conditions was added. Finally, an option was added to the model to simulate plant and root growth under irrigated and nonirrigated conditions, corresponding to experimental conditions at the Auburn rhizotron.

Detailed validation studies, using ROOTSIMU version 4.0 (CSMP-model) and 1981 experimental data, will be published by Hoogenboom et al. (17). For examples presented in this publication, 1983 weather data were used as input functions. The model was run in background mode on a mainframe computer. Although a large amount of CPU time was required, several simultaneous runs, which were needed to calibrate the model, could be executed at the same time. Trial runs on a micro-computer took several hours of actual simulation time. Depending on the resources available, the best performance of the model will be obtained by using the CSMP or ACSL version of the model on either a mainframe or minicomputer.

In these trial simulation runs, $\psi_{\text {canopy }}$ was a critical value in determining total growth. After a rain, upper layers of soil rewet quickly, while water percolated slowly into deeper soil layers until a new equilibrium water potential was established. Plant water potential was high when many roots were present in wet soil, but as soil water reserves diminished,
plant water stress increased. An increasing fraction of soluble carbohydrates was used in the formation of new root tissue as water was depleted from the soil. During the calibration runs of the model, it was observed that under extreme drought conditions plants lost turgor and finally died, usually from carbohydrate starvation because $\mathrm{C}_{2}$ exchange was blocked when stomata could not open due to water stress.

## CONCLUSIONS

Based on calibration runs with the model ROOTSIMU version 4.0, it can be concluded that:

The approach used to handle climatic data provided good algorithms to input real weather data into the model.

The infiltration procedure, together with the Darcian flow equation, was successful in that the predicted below-ground water regime compared reasonably well to experimentally recorded values.

As with the Huck and Hillel (21) version, this model gave plausible indicators of plant response to climatic variables and selected soil variables.

The run time was not excessive on any large system. The model can be run on a personal computer, but considerable time is required.

The simulation languages CSMP and ACSL provided the best languages for running the model.

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APPENDIX A:
CSMP-LISTING OF SIMULATION MODEL


```
ENDMAC
*
**** DAILY TOTALS (DE WIT ET AL.)
*
MACRO DTOT = DLYTOT(DTOTI,RATE)
                DTOT1 = INTGRL(DTOTI,RATE)
                DTOT = DTOT1-ZHOLD(IMPULS((AMAX1(DELT,60.)),86400.)*KEEP,DTOT1)
* THE ACCUMULATOR IS EMPTIED AFTER MIDNIGHT,
* SO CONTENTS ARE AVAILABLE FOR PRINTING
ENDMAC
*
*
MACRO MONTH, J = MTIME(JDAY)
    MONTH = (JDAY/29) + 1
        J = JDAY - DAYS(MONTH)
        IF (J.GE.1) GO TO }77
        MONTH = MONTH - 1
        J = JDAY - DAYS(MONTH)
775 CONTINUE
TABLE DAYS (1-13) =0,31,59,90,120,151,181,212,243,273,304,334,365
* NOTE THAT THE NUMBER OF DAYS AT THE END OF EACH MONTH SHOWN ABOVE
* IS ONLY CORRECT FOR NON-LEAP YEARS. ADD 1 FEB-DEC FOR LEAP YEARS.
ENDMAC
SYSTEM GEN
SYSTEM NPOINT=6000
*DECK
TABLE SMAX(1-6) =. 35, 1.0E10,.004, 2.0,+0.3E-7, 5.0E2
TABLE SMIN(1-6) =.05, -0.5, 0.0, -.1,-0.3E-7, 0.0
* SCALE FACTORS FOR VERTICAL GRADIENT PLOTS
*
*
*
************ INITIALSEGMENT ****************
INITIAL
*
        ZYX = DEBUG(01,0.0)
*
**** LOAD FUNCTIONS FOR REAL WEATHER DATA **
*
PROCEDURE MONTH,DAY,MAXTEM,MINTEM,CMRAIN,RADN,SIMDAY = AAA(TIME)
*
* XX = DEBUG(01,0.0)
* READ(11,511) ISHOOT,IROOT,IDAY,ICHO
* READ(11,512) (ITHETA(I),I=1,11)
* READ(11,512) (RRL(I),I=1,10)
* WRITE (06,511) ISHOOT,IROOT,IDAY,ICHO
* WRITE(06,512) (ITHETA(I),I=1,11)
* WRITE(06,512) (RRL(I),I=1,10)
511 FORMAT(08G10.4)
512 FORMAT(11G07.2)
        JULIAN = START + TIME / 86400.
        SIMDAY = JULIAN
```

```
1853 FORMAT(/,' INITIATE ',/,4X,'SIMDAY',8X,'RADN',7X,'MAXTEM')
* WRITE(6,1853)
    IF (START.GT.400) GO TO 500
FUNCTION MAXTMP
    CALL FGLOAD(MAXTMP,0.,19.,1)
    DO 01 K=1,365
    READ(4,91,END=301) RADN, MAXTEM, MINTEM, CMRAIN, PEVAP ,...
    MAXSTM,MINSTM,SIMDAY
* READ IN HISTORICAL WEATHER RECORDS OF INTEREST
    91 FORMAT(F3.0,1X,F5.1,F6.1,F6.2,F7.3,F3.0,F3.0,T76, F3.0)
        JULIAN = SIMDAY
        JDAY = JULIAN
        MONTH, J = MTIME(JDAY)
        IF (SIMDAY.GT.400) GO TO 101
* WRITE(6,92) SIMDAY, RADN, MAXTEM, MINTEM, CMRAIN, PEVAP,MONTH,...
* MAXSTM,MINSTM,J , JDAY
        92 FORMAT(11G10.4)
    101 MAXTEM = ( MAXTEM - 32. ) * 5. / 9.
        CALL FGLOAD(MAXTMP,JULIAN,MAXTEM,1)
* LOADING INPUT FILES INTO APPROPRIATE FUNCTIONS FOR INTERPOLATION
        Ol CONTINUE
        301 CALL FGLOAD(MAXTMP,400.,MAXTEM,1)
* GO TO 500
    REWIND 4
FUNCTION MINTMP
        CALL FGLOAD(MINTMP,0.,15.,1)
        DO 11 K=1,365
        READ(4,91,END=302) RADN, MAXTEM, MINTEM, CMRAIN, PEVAP ,...
        MAXSTM,MINSTM,SIMDAY
    * READ HISTORICAL WEATHER RECORDS AGAIN (FGLOAD CAN LOAD ONLY ONE
* FUNCTION AT A TIME).
    JDAY = SIMDAY
    JULIAN = JDAY
    MINTEM = ( MINTEM - 32. ) * 5. / 9.
    IF (SIMDAY.GT.200) GO TO 1011
* WRITE(6,92) SIMDAY, MINTEM, JDAY, JULIAN
    1011 CALL FGLOAD(MINTMP,JULIAN,MINTEM,1)
* LOADING OF MINTEM VALUES INTO FUNCTION MINTMP
        11 CONTINUE
    302 CALL FGLOAD(MINTMP,400.,MINTEM,1)
* GO TO 500
        88 REWIND 4
FUNCTION RADFCN
            CALL FGLOAD(RADFCN,0.,100.,1)
            DO 12 K=1,365
            READ(4,91,END=303) RADN, MAXTEM, MINTEM, CMRAIN, PEVAP ,...
            MAXSTM,MINSTM,SIMDAY
* READ HISTORICAL WEATHER RECORDS YET ANOTHER TIME
            JDAY = SIMDAY
            JULIAN = JDAY
            RADN = RADN * 4.2 * 10000
            IF (SIMDAY.GT.365) GO TO 1012
* WRITE(6,92) SIMDAY, RADN, JULIAN, JDAY
    1012 CALL FGLOAD(RADFCN,JULIAN,RADN,1)
```

```
* LOADING OF RADN VALUES INTO FUNCTION RADFCN
    12 CONTINUE
    303 CALL FGLOAD(RADFCN,400.,RADN ,1)
* GO TO 500
    89 REWIND 4
FUNCTION RNFALL
            CALL FGLOAD(RNFALL,0.,0.1,1)
            DO 13 K=1,365
            READ(4,91,END=304) RADN, MAXTEM, MINTEM, CMRAIN, PEVAP ,...
            MAXSTM,MINSTM,SIMDAY
* READ HISTORICAL WEATHER RECORDS YET ANOTHER TIME
            CMRAIN = CMRAIN * 2.54
* CMRAIN = 0.0
            JDAY = SIMDAY
            JULIAN = JDAY
            IF (SIMDAY.GT.200) GO TO 1013
* WRITE(6,92) SIMDAY, CMRAIN, JDAY
    1013 CALL FGLOAD(RNFALL,JULIAN,CMRAIN,1)
* LOADING OF RADN VALUES INTO FUNCTION RADFCN
            13 CONTINUE
    304 CALL FGLOAD(RNFALL,400.,CMRAIN,1)
    5 0 0 ~ C O N T I N U E
            90 REWIND 4
FUNCTION PEV
            CALL FGLOAD(PEV,0.,0.1,1)
            DO 14 K=1,365
            READ(4,91,END=305) RADN, MAXTEM, MINTEM, CMRAIN, PEVAP ,...
            MAXSTM,MINSTM,SIMDAY
* READ HISTORICAL WEATHER RECORDS YET ANOTHER TIME
            PEVAP = PEVAP * 2.54
            JDAY = SIMDAY
            JULIAN = JDAY
            IF (SIMDAY.GT.200) GO TO 1014
    * WRITE(6,92) SIMDAY, PEVAP, JDAY
    1014 CALL FGLOAD(PEV,JULIAN,PEVAP,1)
* LOADING OF PEVAP VALUES INTO FUNCTION PEV
        14 CONTINUE
        305 CALL FGLOAD(PEV,400.,PEVAP,1)
        5 0 1 ~ C O N T I N U E ~
        191 REWIND 4
    FUNCTION MXSTMP
            CALL FGLOAD(MXSTMP,0.,19.,1)
            DO 1115 K=1,365
            READ(4,91,END=306) RADN, MAXTEM, MINTEM, CMRAIN, PEVAP ,...
            MAXSTM,MINSTM,SIMDAY
    * READ IN HISTORICAL WEATHER RECORDS OF INTEREST
            JULIAN = SIMDAY
            JDAY = JULIAN
            MONTH, J = MTIME(JDAY)
            MAXSTM = ( MAXSTM - 32. ) * 5. / 9.
            IF (SIMDAY.GT.200) GO TO 1015
    * WRITE(6,92) SIMDAY, RADN, MAXTEM, MINTEM, CMRAIN, PEVAP,MONTH,...
    * MAXSTM,MINSTM,J , JDAY
    1015 CALL FGLOAD(MXSTMP,JULIAN,MAXSTM,1)
```

```
* LOADING INPUT FILES INTO APPROPRIATE FUNCTIONS FOR INTERPOLATION
    1115 CONTINUE
        306 CALL FGLOAD(MXSTMP,400.,MAXSTM,1)
* GO TO 500
    192 REWIND 4
FUNCTION MNSTMP
            CALL FGLOAD(MNSTMP,0.,15.,1)
            DO 16 K=1,365
            READ(4,91,END=307) RADN, MAXTEM, MINTEM, CMRAIN, PEVAP ,...
            MAXSTM,MINSTM,SIMDAY
* FINAL READING OF HISTORICAL WEATHER RECORDS AGAIN
*
        JDAY = SIMDAY
        JULIAN = JDAY
        MINSTM = ( MINSTM - 32. ) * 5. / 9.
        IF (SIMDAY.GT.200) GO TO 1017
    * WRITE(6,92) SIMDAY, MINTEM, JDAY, JULIAN
    1017 CALL FGLOAD(MNSTMP,JULIAN,MINSTM,1)
    * LOADING OF MINSTM VALUES INTO FUNCTION MNSTMP
        16 CONTINUE
        307 CALL FGLOAD(MNSTMP,400.,MINSTM,1)
* GO TO 500
    193 REWIND 4
*
    JJ = J
        T = MONTH
        TT=T
    * DOUBLE LETTERS ARE REAL NUMBER REPRESENTATION FOR OUTPUT VARIABLES.
*
* ZY= DEBUG(01,0.0)
ENDPRO
*
PARAM PI = 3.14159
PARAM ECON = 2.71828
    RAD = PI/180.
    * STANDARD MATHEMATICAL CONSTANTS
*
    ****** LOCATION TO BE SIMULATED - AUBURN ALA., USA.
    PARAM LAT = 32.5
        CSLT = COS(RAD*LAT)
    * COSINE LATITUDE
        SNLT =SIN(RAD*LAT)
        SINE LATITUDE
*
*
```

```
************RUN CONTROL * * * * * * * * * * * * * * * * * * *
*
TIMER FINTIM= 4320000000., OUTDEL =03600.,PRDEL=3600.,...
    DELT=03600., DELMIN=1.00, DELMAX=3600.
        JULIAN = START + TIME/86400.
* BASIC TIMER UNITS ARE SECONDS. SEE TIME DEFINITIONS IN DYNAMIC SECT.
            OUTF = 3.024E05
* OUTPUT FUNCTION FOR VERTICAL GRADIENT PLOTS MADE DURING EXECUTION --
* --INITIAL FREQUENCY FOR VERTICAL GRADIENT PLOTS IS INCREMENTED LATER.
*
*FINISH HOURS=2160.,POTCR= -300., SOLCHO = +1.0E-07, SHOOTW=0.0001, ...
FINISH HOURS=2400.,POTCR= 460., SOLCHO = +1.0E-07, SHOOTW=0.0001, ...
    TOPGRO = -1.0E-10, TOTRG = -1.0E-18,JULIAN=365.
* THE SIMULATION WILL TERMINATE WHEN THE PLANT WATER POTENTIAL DROPS
* BELOW -460 METERS WATER POTENTIAL (OR -4.5 MPA) (BOYER, 1970),
* OR WHENEVER SOLUBLE CARBOHYDRATE IS EXPENDED (NO FOOD IN STORAGE).
            MTH = MONTH - 0.5 + ((DAY/30))
* REAL-NUMBER REPRESENTATION OF MONTH, FOR INDEXING TABULAR FUNCTIONS.
*
*METHOD RECT
METHOD RKS
RELERR SOLCHO = 1.0E-02
ABSERR SOLCHO = 1.0E-02
RELERR POTCRD = 1.0E-01
ABSERR POTCRD = 1.0E-01
ABSERR LSNHS = 0.1
RELERR LSNHS = 0.1
RELERR SHOOTW = 1.0E-04
ABSERR SHOOTW = 1.0E-04
RELERR CUMRAD = 1.0E-03
ABSERR CUMRAD = 1.0E-03
* SPECIFICATION OF CONVERGENCE CRITERIA FOR VARIABLE TIME-STEP INTGRLS
*
*
    RUNS = 0
    FLPFLP = -1.0
PARAMETER ERROR = 0.01
PARAMETER CF = 0.10
* CORRECTION FACTOR AND ERROR PARAMETERS FOR ITERATIVE LOOP
*
* ** INITIATION OF PLANT-GROWTH PARAMETERS
*
PARAM IPER = 0.03
    ICHO = (ISHOOT + IROOT) * IPER / ( 1. - IPER )
* INITIAL CARBOHYDRATES (KG/M**2), AS DECIMAL FRACTION OF TOTAL WGT.
PARAM ISHOOT = 10.0E-03
PARAM IROOT = 02.00E-03
* INITIAL SHOOT AND ROOT WEIGHTS, RESPECTIVELY (KG/M**2)
    DRYWT = ISHOOT + IROOT
    STEMW = STWTR * ISHOOT
    LEAFW = ISHOOT - STEMW
    LAI = LEAFW * LEAFTH
    IRTL = IROOT * LNGFAC
```

```
* METERS OF ROOT/SQUARE METER GROUND AREA AT INITIATION
PARAM RTDWPC = 10.
* PERCENTAGE DRY MATTER OF ROOTS
PARAM LNGFAC = 13000.0
* LENGTH FACTOR, AS METERS OF ROOT PER KG ROOT WEIGHT
* (A FACTOR OF 1000 CORRESPONDS TO ABOUT 1 MM ROOT DIAMETER)
* LEAF AREA INDEX -- AREA OF LEAF SURFACE/UNIT LAND AREA
TABLE RRL(1-10) = 0.54, 0.38, 0.08, 0.00, 0.0, ...
    0.0 , 0.0, 0.0, 0.0, 0.0
*TABLE RRL(1-10)=2.7E-01, 2.5E-01, 2.4E-01, 2.1E-01, 0.03, ...
* .00, 0.0, 0.0, 0.0, 0.0
* RELATIVE ROOT LENGTH (AS FRACTION OF TOTAL)
            Cl=2
            C2=1
            O1=2
            02=1
*
* ** INITIATION OF WATER-BALANCE PARAMETERS
*
TABLE ITHETA(1-11) = 0.200, 0.200, 0.200, 0.200, 0.200, ...
    0.200, 0.200, 0.200, 0.200, 0.230,0.300
* INITIAL SOIL WATER CONTENT (VOLUME FRACTION)
* (INITIATED TO VALUES FOUND AFTER 12 DAYS OF DRAINING FROM
* SATURATION AT 20% WATER IN ALL LAYERS)
*
PARAM STHETA = 0.36
    SATCON = 5.00E-03/100
*PARAM SATCON = 10.00E-03 / 100
* SATURATED CONDUCTIVITY, AS M/SEC
            ETA = 2.0 + 3.0* ZLAM
PARAM ZLAM = 0.64762
* Z(LAMBDA), AFTER LALIBERTE, BROOKS, & COREY
PARAM ALPHA = 0.24890
PARAM NU = 1.21555
    MU = 1 - ( 1 / NU )
* A,N,M FOR HYDRAULIC CONDUCTIVITY CALCULATIONS AFTER VAN GENUCHTEN,1978
PARAM PARTDS = 2.59
* PARTICLE DENSITY
FUNCTION BULKF = ((0.0,1.52),(1.0,1.52),(2.0,1.52))
* BULKDENSITY AS A FUNCTION OF DEPTH
TABLE TCOM(1-20) =. 10, 2 *. . 15, 17 *. 20
* THICKNESS OF EACH VERTICAL LAYER (COMPARTMENT), METERS
*
NOSORT
**PROCEDURE DEPTH,DIST,PRTL,RSRT,IVOLW = INTLZ(TCOM,RRL)
* ZYX = DEBUG(01,0.0)
PARAM NJ = 10
    NJJ = NJ+1
* ONE MORE THAN THE NUMBER OF LAYERS IN THE SOIL PROFILE (NJ)
    NNJ = NJ - 1
* ONE LESS THAN THE NUMBER OF LAYERS IN THE SOIL PROFILE (NJ)
    DO 15 I = 1,NJJ
    15 FLW(I) = 0.0
* FLOW OF WATER PAST BOTTOM OF EACH LAYER, INITIATED TO 0.0
```

```
* THE NUMBER OF LAYERS(J) IN THE SOIL PROFILE
    DEPTH(1) = .5*(TCOM(1))
    DIST(1) = DEPTH(1)
    IVOLW(1) = ITHETA(1)*TCOM(1)*1.0
    DO 20 I = 2,NJJ
        DIST(I) = . 5*(TCOM(I-1)+TCOM(I))
        DEPTH(I) = DEPTH(I-1) + DIST(I)
        IVOLW(I) = ITHETA(I)*TCOM(I)*1.0
* INITIAL VOLUME OF WATER IN EACH SOIL LAYER
    20 CONTINUE
    853 FORMAT(/,' INITIATE ',/,9X,'I',3X,'IPRTL',5X,'RSRT',8X,'IVOLW')
        WRITE(6,853)
* 853 format(/, ' inItIATION ', /, 8X, 'I', 5x, 'IPRTL', 5x, ...
* 'RSAT', 6X, 'IVOLW', 5X, 'TCOM', 4X, 'ITHETA', 5X, 'IRTL', ...
* 6x, 'RRL', 5x, 'DEPTH', /)
    DO 30 I = 1,NJ
    IPRTL(I) = IRTL * RRL(I)
* partial root length, at initiation
    IRTWT(I) = IPRTL(I) / LNGFAC
* ROOT WEIGHT, AT INITIATION
    IRTVL(I) = IRTWT(I) * 100. / (RTDWPC*1000)
* ROOT VOLUME, AT INITIATION
        RRS(I) = URRS / (IPRTL(I) +NOT(IPRTL(I))*1.0E-10)
* RADIAL RESISTANCE TO WATER FLOW IN THE ROOT
        ARS(I) = UARS * DEPTH(I) / (IPRTL(I) + NOT(IPRTL(I))*1.0E-10)
* AXIAL RESISTANCE -- ALONG THE XYLEM TRANSPORT SYSTEM
        RSRT(I) = RRS(I) + ARS(I)
* RESISTANCE OF THE ROOTS
        WRITE(6,454) I,IPRTL(I),RSRT(I),IVOLW(I),TCOM(I),ITHETA(I), ...
                IRTL, RRL(I), DEPTH(I)
    454 FORMAT(3G10.3, 3F10.5, G10.3, 2F10.5, 3G10.3)
        30 CONTINUE
**ENDPRO
*
        POTCR = -20.000
* POTENTIAL OF THE CROWN (SHOOT), INITIATED BELOW DRIEST SOIL LAYER
* (-20 METERS = -0.2 MPA)
*
FUNCTION SUTB = (0.00,60.),(0.0674,40.81),(0.0940,21.21),\ldots.
(0.1119,15.27),(0.1263,7.325),(0.1363,4.11),(0.1531,2.01),\ldots.
(0.1705,0.99),(0.2063,0.425),(0.2461,0.264),\ldots
(0.36,0.0),(0.42,0.0),(0.50,0.0)
* IN - SITU RHIZOTRON DATA 1982
NOSORT
        DO 10 I = 2,101
        10 LINE(I) = IB
* INITIATES PRINT-LINE FOR VERTICAL PLOTS TO BLANK CHARACTER-STRING
*
*
    ZZZ = DEBUG(01,0.0)
*
```

```
** * * * * * * * * * * DYNAMIC SEGMENT * * * * * * * * * * * * * * *
DYNAMIC
*
*
* YYY =DEBUG(100,1359000.)
* ZZ = DEBUG(01,86400.)
*
*
** ** TIME CALCULATIONS **
PARAM START = 150.
* BEGINNING DATE FOR THIS SIMULATION RUN
        JULIAN = START + TIME/86400.
        DAY = JULIAN
* JULIAN DATE OF SIMULATION
        JDAY = JULIAN
* INTEGER REPRESENTATION OF JULIAN DAY, FOR INPUT TO mTIME
PROCEDURE MONTH, J = AAA(JDAY)
        MONTH, J = MTIME(JDAY)
ENDPRO
*
        T = MONTH
        TT = T
* INTEGER AND REAL-NUMBER REPRESENTATIONS, RESPECTIVELY.
        MTH = MONTH - 0.5 + ((AGE/30))
* REAL-NUMBER REPRESENTATION OF MONTH, FOR INDEXING AND OUTPUT
*
        JJ = J
* CALENDAR dAY OF THE MONTH
        AGE = HOURS / 24.00
    DAYS OF SIMULATION (CUMULATIVE, SINCE BEGINNING OF RUN).
*
        HOURS = TIME/3600.0
* CUMULATIVE HOURS OF SIMULATION TIME
        HOUR = AMOD(HOURS,24.0)
* CLOCK TIME, IN HOURS
        RUN = RUNS
* CREATES A REAL-NUMBER COUNTING VARIABLE FOR PRINTER OUTPUT
*
* DIRECTION OF THE SUN
        DEC = -23.4*COS(2.*PI*(JULIAN+10.)/365.)
        DECLINATION OF THE SUN
        SNDC = SIN(RAD*DEC)
        SINE DECLINATION
        CSDC = COS(RAD*DEC)
* COSINE DECLINATION
        SNHSS=SNLT*SNDC+CSLT*CSDC*COS(PI*(HOUR+12.)/12.)
* SINE OF THE HEIGHT OF THE SUN
        LSNHS=INTGRL(-0.5,(SNHSS-LSNHS)/DELT)
* SUN HEIGHT AT lAST TIME STEP
        RISE = ZHOLD(AND(SNHSS,-LSNHS)-0.5,HOUR-SNHSS*DELT/
                                    ((NOT(SNHSS-LSNHS)+SNHSS-LSNHS)*3600.)-RISEI)+RISEI
* TIME OF SUN RISE TODAY, IN HOURS, ESTIMATED FOR TOMORROW
INCON RISEI = 4.8
*
```


## PA

* DELAY FUNCTION, BASED UPON SOIL HEAT CAPACITY (HALF-TIME FOR
* EQUILIBRATION, IN RECIPROCAL SECONDS).
TMPFCS $=10.0 * *(($ TEMP-REFT $) * 0.030103)$
TMPFCR $=10.0 * *(($ STEMP-REFTS $) * 0.030103)$
BIOLOGICAL Q-10 -- DOUBLING REACTION RATE AT EACH 10 DEGREE TEMP CHNG
TEMP = WAVE (JULIAN, HOUR, MINTMP, MAXTMP, RISE)
AIR TEMPERATURE, AS DEGREES C.
REFT $=25$.
AVAT $=$ (MAXTEM + MINTEM) $* 0.500$
AVERAGE AIR TEMPERATURE, FROM DAILY MEASUREMENT DATA
MAXTEM $=$ AFGEN (MAXTMP, JULIAN-(14./24.))
MINTEM = AFGEN(MINTMP,JULIAN-(RISE/24.))
LINEAR INTERPOLATION FROM INPUT DATA-FILE
RANGE $=$ (MAXTEM - MINTEM) $* 0.500$
AIR TEMPERATURE, AS DEGREES C.
STEMP = WAVE((JULIAN-0.16), (HOUR-4.), MNSTMP,MXSTMP,RISE)
REFTS $=25$.
AVST $=$ (MAXSTM + MINSTM) $* 0.500$
AVERAGE SOIL TEMPERATURE, FROM DAILY MEASUREMENT DATA
MAXSTM $=$ AFGEN (MXSTMP, JULIAN-(14.+4.)/24.)
MINSTM $=$ AFGEN (MNSTMP, JULIAN-(RISE+4.) /24.)
LINEAR INTERPOLATION FROM INPUT DATA-FILE
RANGES $=($ MAXSTM - MINSTM $) * 0.500$
AMPLITUDE OF DAILY TEMPERATURE OSCILLATIONS
EQUILIBRATION, IN RECIPROCAL SECONDS).
** RESERVE LEVELS AND TISSUE GROWTH **
RESL $=$ SOLCHO / (SOLCHO + ROOTW + SHOOTW)
RESERVE LEVEL, \% FREE CARBOHYDRATE IN TISSUES
SOLCHO $=$ INTGRL (ICHO, (PHOTSN * PHTCAR - GROWTH - RESP) $)$
PHTCAR $=30 . / 44$.
SOLUBLE CARBOHYDRATES (FREELY MOBILE, AS METABOLIC RESERVES)
(KG/SQUARE METER)
GROWTH $=$ TOPGRO + TOTRG
TOTAL GROWTH OF BOTH SHOOT AND ROOT SYSTEM
** ESTIMATION OF RADIATION INTENSITY **
CUMRAD $=$ INTGRL(0.,RADN/86400.)
DAYRAD $=(1-\operatorname{IMPULS}(0 ., 86400)). * \operatorname{INTGRL}(0 ., \operatorname{RADN} / 86400$.
CUMULATIVE TOTAL RADIATION RECEIVED--COMPARE WITH INPUT VALUES.
RADN $=\operatorname{AMAX1}(0.0, \operatorname{SIN}(2 * P I *(D A Y-0.250))) *$ MAXRAD $* 3.0$
RADIATION INTENSITY (INSTANTANEOUS VALUE)
FACTOR OF 3.0 PUTS ABSOLUTE VALUE ON SCALE WITH RIGHT UNITS
MAXRAD $=$ AFGEN (RADFCN,JULIAN) $/ 86400$.

```
* RADIATION INTENSITY, INTERPOLATED FROM INPUT FILE
    SNHS = AMAXI(0.,SNHSS)
    HSUN = ATAN(SNHS/SQRT(1.-SNHS*SNHS))/RAD
    DIFOV = AFGEN(DFOVTB,HSUN)
FUNCTION DFOVTB = (0.,0.),(5.,6.),(15.,26.),(25.,45.),(35.,64.),...
    (45.,80.),(55.,94.),(65.,105.),(75.,112.),(90.,116.)
* DIFFUSE OVERCAST VISIBLE
    DIFON = 0.7 * DIFOV
* DIFFUSE OVERCAST INFRARED
    DIFCL = AFGEN(DFCLTB,HSUN)
FUNCTION DFCLTB = (0.,0.),(5.,29.),(15.,42.),(25.,49.),(35.,56.),\ldots
            (45.,64.),(55.,68.),(65.,71.),(75.,75.),(90.,77.)
* DIFFUSE CLEAR
    SUNDCL = AFGEN(SUNTB,HSUN)
FUNCTION SUNTB = (0.,0.),(5.,0..),(15.,88.),(25.,175.),(35.,262.),\ldots
            (45., 336.),(55.,402.),(65.,452.),(75.,483.),(90.,504.)
* DIRECT CLEAR
    CRC = (SUNDCL+DIFCL)*2.
* CURRENT RADIATION CLEAR, ALL WAVELENGTHS
    CRO = DIFOV + DIFON
* CURRENT RADIATION, OVERCAST
    DRC = DLYTOT(DRCI,CRC)
    DRO = DLYTOT(DROI,CRO)
INCON DROI = 6.6E6
INCON DRCI = 3.5E7
    DRCP = ZHOLD(IMPULS(0.,86400.),DRC)
    DROP = ZHOLD(IMPULS(0.,86400.),DRO)
    DTRR=AFGEN(RADFCN,(JULIAN-0.0))
    DTR = ZHOLD(IMPULS(0.,86400.)*KEEP,DTRR)
    FCL = (DTR - DROP)/(NOT(DRCP-DROP)+DRCP-DROP)
    FOV = 1. - FCL
    LFOV = LIMIT(0.,1.,FOV)
    LFCL = 1. - LFOV
    RADIAT = LFCL * CRC + LFOV * CRO
    DRAD = DLYTOT(DRADI,RADIAT)
INCON DRADI = 1.E-10
*
*
* ** PHOTOSYNTHETIC ACTIVITY **
*
*PARAM MXPHOT = 0.6944E-6
PARAM MXPHOT = 0.8200E-6
* MAXIMUM PHOTOSYNTHETIC RATE - 25 MG CO2 DM-2 (LEAF) H-1
PARAM DKPHOT = 0.
* NET ASSIMILATION IN THE DARK - DARK RESPIRATION OF THE LEAVES
    RADCPH = 0.5 * CRC
    RADOPH = 0.5* CRO
* PHOTOSYNTHETIC ACTIVE RADIATION
PARAM EFF = 0.01388E-6
*EFFICIENCY AT THE LIGHT COMPENSATION POINT - 0.5 KG CO2 J-1 HA-1 H-1 M2
    SLLA = AMIN1(LAI, 2*SNHS)
* SUNLIT LEAF AREA
    DLLA = LAI - SLLA
```

```
* TOTAL LEAF AREA IN THE SHADE
    XOVC = RADOPH * EFF / ( MXPHOT * LAI )
    POVC = XOVC / ( XOVC + 1. )
    PHOTD = LAI * MXPHOT * POVC
* MAXIMUM CANOPY PHOTOSYNTHESIS UNDER AN OVERCAST SKY
    XS = ALOG ( 1+(0.45 * EFF*RADCPH/(AMAX1(SLLA,0.0001)*MXPHOT)))
    PS = XS / ( 1 + XS )
    PHOTS = SLLA * MXPHOT * PS
* MAXIMUM CANOPY PHOTOSYNTHESIS UNDER A CLEAR SKY FOR SUNLIT LEAFAREA
    XSH = ALOG( 1+(0.55* EFF * RADCPH/(AMAXI(DLLA,0.0001)*MXPHOT)))
    PSH = XSH / ( 1 + XSH )
    PHOTSH = DLLA * MXPHOT * PSH
* MAXIMUM CANOPY PHOTOSYNTHESIS UNDER A CLEAR SKY FOR SHADED LEAFAREA
PROCEDURE PHOTC,PHOTSN,PHOTSM=PROCPH(PHOTS, PHOTSH,PHOTD,WATRST,TMPFCS)
    PHOTC = PHOTS + PHOTSH
    IF ( LAI .GT. 03) GO TO 31
    IF ( RADIAT .EQ. 0 ) GO TO 31
    FINT = ( 1. - EXP(-0.8*LAI ))
    Cl = FINT * PHOTC
    C2 = LAI * MXPHOT
    O1 = FINT * PHOTD
    O2 = C2
    IF ( C1 .GT. C2 ) GO TO 32
    C0 = C1
    C1 = C2
    C2 = C0
    32 CONTINUE
    PHOTC = C2 * ( 1. - EXP ( - C1 / (NOT(C2)+C2) ))
    IF ( O1 .GT. O2 ) GO TO 33
    O0 = 01
    01=02
    O2=00
    33 CONTINUE
    PHOTD = O2 * ( 1. - EXP ( - O1 / (NOT(O2)+02) ))
    31 CONTINUE
    PHOTSN = WATRST * ( PHOTC * LFCL + PHOTD * LFOV)
    PHOTSM = ( 1.- IMPULS(1800.,86400.))*AMAX1(PHOTSN,PHOTSM)
* PHOTOSYNTHETIC RATE (NET CARBON FIXATION, KG/SQUARE METER/SECOND
ENDPRO
*
*
* ** ROOT AND SHOOT RESPIRATION **
*
    RESP = RESPSH + RESPRT
* TOTAL RESPIRATION, INCLUDING BOTH SHOOT AND ROOT SYSTEM
    RESPSH = SHMRES + SHGRES
* RATE OF SHOOT RESPIRATION (KG/SQ METER/SEC)
* (SUM OF GROWTH RESPIRATION AND MAINTENANCE RESPIRATION)
    SHMRES = SHOOTW * TMPFCS * RSPFAC
    CSTMRS = INTGRL( 0.0,SHMRES)
* SHOOT MAINTENANCE RESPIRAATION
PARAM RSPFAC = 1.0E-07
* RESPIRATION FACTOR, CONVERTING UNITS AND PROPORTIONING
    SHGRES = TOPGRO * CONVRT
```

```
* SHOOT GROWTH RESPIRATION
PARAM CONVRT = 0.30
* CONVERSION EFFICIENCY (WEIGHT OF TISSUE PRODUCED PER GRAM INPUT
* (INCLUDES RESPIRATION FOR TRANSPORT AND CHEMICAL CONVERSIONS)
*
RESPRT = RTMRES + RTGRES
* RESPIRATION OF ROOT SYSTEM
RTMRES = ROOTW * RSPFAC * TMPFCR
CRTMRS = INTGRL(0.0,RTMRES)
* ROOT MAINTENANCE RESPIRATION
    RTGRES = TOTRG*CONVRT
* ROOT GROWTH RESPIRATION, INCLUDING CHEMICAL CONVERSION AND TRANSPORT
*
* ** GROWTH AND DEATH OF SHOOT TISSUE **
*
    SHOOTW = INTGRL(ISHOOT, (TOPGRO - SHOOTD))
* WEIGHT OF LIVING SHOOT TISSUE (KG/SQ METER)
*
    TOPGRO = TMPFCS * GROFAC * SOLCHO * FRAC
    TOPGRO = TMPFCS * GROFAC * SOLCHO * FRG
* RATE AS (KG/SQ METER/SEC) OF SHOOT (STEMS, LEAVES, AND FRUIT)
* FRAC = AFGEN(FRACTB,POTCR)
    FRAC = AFGEN(FRACTB,POTCRE)
* FRACTIONAL GROWTH, AS PERCENT OF CARBON GOING INTO THE SHOOT
    POTCRE = AMIN1(POTCR, POTCRD)
* EFFECTIVE CANOPY WATER POTENTIAL
    POTCRD = INTGRL(10.,(POTCR - POTCRD)/DELAY)
* DELAYED CANOPY WATER POTENTIAL
*PARAM DELAY = (21600., 1800.)
PARAM DELAY = 21600.
* DELAY TIME FOR COMPUTING OF POTCRD, IN SECONDS
PARAM FRG = 0.666
*PARAM FRG = (0.0, 1.0, 0.666)
* FRACTION OF CARBOHYDRATES GOING TOWARD SUPPORT OF SHOOT GROWTH
FUNCTION FRACTB = -500.,.05, -200.,.20, -050.,.65, -05.,.90, ...
    100.,.90
* UNITS = %, AS A FUNCTION OF CANOPY WATER POTENTIAL, POTCR
*
*
    SHOOTD = LEAFW * TMPFCS * DTHBGN * AGING
* SHOOTD = SHOOTW * TMPFCS * DTHBGN * AGING
* SHOOT DEATH RATE (PRINCIPALLY LEAF-DROP DUE TO AGE AND WATER STRESS)
    DTHBGN = AFGEN(DTBL, LAI)
* LEAVES BEGIN DYING AS LAI INCREASES ABOVE 2, DUE TO SELF-SHADING
FUNCTION DTBL = 0.0,0.0, 2.0,0.03, 5.0,0.33, 07.0,0.97,10.,1.00,25.,1.0
    AGING = AGFAC * (AGE/30.)
*PARAM AGFAC = 3.0E-7
PARAM AGFAC = 3.0E-07
*
    DRYWT = SHOOTW + ROOTW
    STEMW = STWTR * SHOOTW
    LEAFW = SHOOTW - STEMW
PARAM STWTR = 0.25
    LAI = LEAFW * LEAFTH
```

        ROOTW = INTGRL(IROOT, (TOTRG-ROOTDY))
    * WEIGHT OF LIVE ROOT TISSUE (ALL SOIL LAYERS)
ROOTL $=$ ROOTW * LNGFAC
* LENGTH OF LIVE ROOT TISSUE (ALL SOIL LAYERS)
TOTRG $=(1.0-$ FRAC $) * S O L C H O *$ GROFAC * TMPFCR
TOTRG $=(1.0-$ FRG $) *$ SOLCHO $*$ GROFAC $*$ TMPFCR
* TOTAL ROOT GROWTH, SUM OF ROOT WEIGHT IN ALL SOIL LAYERS
PARAM GROFAC $=1.0 \mathrm{E}-05$
* RELATIVE CONSUMPTION RATE FOR RESERVES -- AFTER DE WIT:
* (GROWTH FACTOR, CONVERTING SOLUBLE CARBOHYDRATE TO TISSUE BIOMASS)
*       ROOTDY = ROOTW / RESL* DTHFAC * TMPFCR
    * RATE OF DYING FOR TOTAL ROOT SYSTEM -- MODULATED IN SUMMATION OF
* DEATH RATES FOR ROOTS IN EACH SOIL LAYER IN A LATER SECTION.
* INVERSELY PROPORTIONAL TO CARBOHYDRATE RESERVES--DYING OFF WHEN HUNGRY
* (RATE EXPRESSED AS KG ROOTS/SQUARE METER/SECOND - - WHOLE PLANT)
PARAM DTHFAC $=1.0 \mathrm{E}-08$
$\because$ PARAM DTHFAC $=(1.0 \mathrm{E}-07,1.0 \mathrm{E}-09,1.0 \mathrm{E}-05)$
* FACTOR TO SCALE ROOT DEATH RATE
* 
* 
* $* *$ TRANSPIRATION **
$*$
TRANSP $=1.0 *$ WATRST $*$ PET * LAIFAC
* TRANSPIRATION LOSSES, AS METER/SECOND
WATRST $=$ AFGEN (TRNTBL, POTCR)
* WATER STRESS IN PLANT TISSUE
* 

FUNCTION TRNTBL $=-500 ., .05,-245 ., .05,-163 ., 0.50,-112 ., 0.95,0 ., 1.0$

* TRANSPIRATION TABLE FOR SOYBEAN ( BOYER, 1970)
*FUNCTION TRNTBL $=-500 ., .05,-200 ., .05,-010 ., 0.95,0 ., 1.0,100 ., 1.0$
* TRANSPIRATION TABLE FOR SUCCULENT CROPS SUCH AS MAIZE
*FUNCTION TRNTBL $=-500 ., 0 .,-400 ., 0.02,-300 ., 0.06, \quad .$.
* -150.,0.75, -50.,0.96, 0.,1.00, +200.,1.00
* TRANSPIRATION TABLE FOR DROUGHT-TOLERANT CROPS-EG. COTTON OR SORGHUM
* LAIFAC $=$ AFGEN(LAITBL,LAI)
* LEAF AREA INDEX FACTOR, PARTITIONS WATER LOSS BETWEEN PLANT \& SOIL
FUNCTION LAITBL =
$0 ., 0 ., 2.0,0.5,4.0,0.8,6.0,0.9,10.0,0.95,25 ., 0.95$
* 

```
**
*
        WATER = ZHOLD(IMPULS(0.,86400.)*KEEP,RNF)
        RAIN = WATER / 86400.
        DAYRAI = DLYTOT(DRADI,RAIN)
* CUMULATIVE SUM OF WATER ADDED BY RAINFALL--COMPARE WITH WEATHER DATA
        RNF = AFGEN(RNFALL,JULIAN) * 0.01
* RAINFALL (M) OCCURRING ON THIS DATE, IN UNITS OF CM/DAY
*
        PET =AMAX1(PEVV * 0.01 / 86400., RADIAT * PEVVV /...
                        (AMAX1(0.01,DTR * 1.0 )))
    POTENTIAL EVAPOTRANSPIRATION, BASED ON TEMPERATURE (& RADIATION)
        (NOT LESS THAN 1% OF AVERAGE TRANSP. DEMAND--NEGATIVES ELIMINATED)
        CUMPET = DLYTOT(DRADI,PET)
* CUMULATIVE POTENTIAL EVAPOTRANSPIRATION -- COMPARE OUTPUT WITH AVPET
*
        PEVV = AFGEN(PEV,JULIAN) * 0.01
* MEASURED POTENTIAL EVAPOTRANSPIRATION IN FIELD (METER PER DAY)
        PEVVV = ZHOLD(IMPULS(0.,86400.)*KEEP,PEVV)
        SLEVAP = PET * (1.0 - LAIFAC) * 1.0
    SOIL EVAPORATION (METER/SEC), PET REDUCED BY LEAF SHADING
                *** SOIL WATER MOVEMENT CALCULATIONS **
        VOLW = INTGRL (IVOLW , NFLW , 12)
        VOLUME OF WATER STORED IN EACH SOIL LAYER
            *** COMPUTE SOIL WATER CONTENT, POTENTIALS, AND CONDUCTIVITY
NOSORT
*PROCEDURE THETA, POTM, POTH, MPOT, RK, COND, C, D, E, F, G, H ...
* = PROCl(TIME, PB)
* IRRIGATION SYSTEM
PARAM IRFAC = 10.
    IRMIN = 10.2118* IRFAC / 100.
    PULSIR = IMPULS(0.0,1800.)
PARAM IRQUAN = (0.0,250.0)
*PARAM IRQUAN = 250.0
            PULSSW = INSW((IRMIN+POTM(3)),(IRQUAN*1.0E-6),0.)
    VOLW(1) = VOLW(1) + RAIN * DELT + PULSSW * PULSIR
* VOLW(NJJ) = TCOM(NJJ) * 0.30
    DO 100 I = 1,NJJ
    BULKDS(I) = AFGEN(BULKF,DEPTH(I))
    POROS(I) = 1 - (BULKDS(I) / PARTDS)
* POROSITY OF EACH SOIL LAYER
        THETA(I) = VOLW(I)/TCOM(I)
        DRAING = (AMAX1(0.0,THETA(NJJ)-STHETA))*TCOM(NJJ)/DELT
        THETA(I) = AMIN1(THETA(I),STHETA)
        VOLW(I) = THETA(I) * TCOM(I)
        POTM(I) = -AFGEN(SUTB,THETA(I))
        POTH(I) = POTM(I) - DEPTH(I)
    100 CONTINUE
* WRITE (6, 854)(POTM(J),J=1,NJ)
```

```
*
* ** COMPUTE SOIL HYDRAULIC CONDUCTIVITY **
*
    DO 85 I = 1, NJJ
    MPOT = -POTM(I) * 100.0
    IF (MPOT.LE. 0.0) GO TO 84
PARAM PB = 21.8258
* BUBBLING PRESSURE (AIR ENTRY VALUE FOR TOPSOIL)
AH = ALPHA * MPOT
RK(I)=(1-(AH)**(NU-1)*(1+(AH)**NU)**(-MU))**2/
((1+(AH)**NU)**(MU/2))
* RELATIVE CONDUCTIVITY (AS A FRACTION OF SATURATED CONDUCTIVITY)
            GO TO }8
        84 RK(I) = 1.0
* RELATIVE CONDUCTIVITY CAN NEVER BE MORE THAN 1.0;
* THUS, SATURATED CONDUCTIVITY APPLIES IF MATRIC POTENTIAL IS POSITIVE
    87 CONTINUE
* WRITE(6,854) I, MPOT, RK(I), AH, JDAY
    854 FORMAT(12G10.3)
        RK(I) = AMIN1(1.00, RK(I))
* CONDUCTIVITY IS LIMITED TO A MAXIMUM OF THE SATURATED CONDUCTIVITY
        COND(I) = RK(I) * SATCON
        COND(I) = RK(I) * SATCON / 8.6400E06
* SOIL HYDRAULIC CONDUCTIVITY, METERS/SECOND
    85 CONTINUE
        WRITE (6, 854)(RK(J), J=1,NJ)
        WRITE (6, 854)(COND(J),J=1,NJ)
*
*ENDPRO
*
* ** COMPUTE VERTICAL SOIL WATER FLOW (DARCIAN) **
*
*PROCEDURE AVCOND, FLW, NFLW , CC, DD, EE = PROC2(POTH,FF)
        DO 110 I = 2,NJJ
        AVCOND}(I)=.5*(COND(I-1)+COND(I)
        FLW(I) = AVCOND(I) * (POTH(I-1)-POTH(I)) / DIST(I)
    110 CONTINUE
        FLW(NJJ+1) = DRAING
        NFLW(NJJ+1) = DRAING
PARAM THTAIR = 0.050
        POTMAR = - AFGEN(SUTB,THTAIR)
        IF (POTM(1) .GT. POTMAR) FLW(1)=-SLEVAP
        IF (POTM(1) .LE. POTMAR) FLW(1)=FLW(2)
* WATER FLOW OUT THE TOP IS LIMITED BY SUPPLY IF TOP LAYER IS DRY
        DO 120 I = 1,NJJ
            NFLW(I) = FLW(I) - FLW(I+1) - RTEX(I)
    120 CONTINUE
*ENDPRO
*
* ** PARTITIONING AGGREGATE ROOT GROWTH BETWEEN SOIL LAYERS **
*
*PROCEDURE BIRTH,EXTENS,RTGRO,SUMRG,RTDTH,SUMRD,NETGRO, ...
* W, AAA,BBB,CCC,DDD,EEE,FFF,GGG,SUMRTG,SUMRTD = PROC3(POTM,HHH)
*
```

```
*
*
*PARAM BRMIN = -1.00
*PARAM EXTMIN = -2.00
PARAM BRMIN = -1.00
PARAM EXTMIN = -2.00
* THRESHOLD POTENTIAL, THE DRIEST SOIL IN WHICH ROOT GROWTH CAN OCCUR
*
    W = AMAX1(0.0, (POTM(2) - EXTMIN))
    DO 1010 I=1,NNJ
    X = AMAX1(0.0, (POTM(I) - BRMIN))
    XX = AMAXI(0.0, (POTM(I) - EXTMIN))
PARAM DEPTHG = 10.
    BIRTH(I) = (BR*(1.0-EXP(-AA*X**BB ) ) )/(((DEPTH(I)*DEPTHG))**1.)
PARAM BR = 1.0E-04
*PARAM BR = 1.0E-08
* BRANCHING RATE, FOR NEW ROOT GROWTH IN THE SAME SOIL LAYER
                                    EXTENS(I)=(EXTNRT*(1.0-EXP (-AA*XX**BB)))/(((DEPTH(I)*DEPTHG))**1.)
    IF ( PRTL(I) .LT. MINRTL * TCOM(I)) EXTENS(I) = 0.
PARAM MINRTL = 5.
PARAM EXTNRT = 3.0E-03
* EXTENSION RATE, FOR NEW ROOT GROWTH FROM ONE LAYER INTO THE NEXT,
* IN UNITS OF METERS/SECOND
PARAM AA = 8.0E-3
PARAM BB = 2.0
* COEFFICIENTS FOR SIGMOID ROOT GENERATION CURVES
*
    1010 CONTINUE
        RTGRO(1) = PRTL(1) * BIRTH(1) * (1.0 - FRAC) * TMPFCR
        SUMRG = RTGRO(1)
* SUMMATION OF INSTANTANEOUS ROOT GROWTH RATES, OVER ALL SOIL LAYERS
* (EXPRESSED AS METERS ROOTS/SQUARE METER SURFACE/SECOND)
            DO 647 I = 2,NNJ
            RTGRO(I) = (PRTL(I-1)*EXTENS(I-1) + PRTL(I)*BIRTH(I)) * ...
            (1.0 - FRAC) * TMPFCR
* RTGRO(I) = (PRTL(I-1)*EXTENS(I) + PRTL(I)*BIRTH(I))
* GROWTH EXPRESSED AS METERS/SEC IN EACH SQUARE METER OF EACH LAYER
* RTGRO(NNJ) = 0.0
            SUMRG = RTGRO(I) + SUMRG
    6 4 7 \text { CONTINUE}
            RTGRO(NJ) = 0.0
* TOTAL INCREASE, WHOLE PLANT, IN METERS/SQ. METER/SECOND
*
            SUMRTG = 0.0
            DO 648 I = 1,NNJ
            IF (SUMRG.EQ.0.00) GO TO 648
            RTGRO(I) = RTGRO(I) * TOTRG/SUMRG * LNGFAC
* (BRINGS ACTUAL ROOT GROWTH IN EACH LAYER INTO LINE WITH TOTAL
* PHOTOSYNTHATE AVAILABLE AT ANY GIVEN TIME).
            SUMRTG = SUMRTG + RTGRO(I)
    6 4 8 \text { CONTINUE}
*
    IF (YY .GT. 0.0) GO TO 751
    IF (TIME.GT.300) GO TO 127
```

```
    751 CONTINUE
* WRITE(6, 852)
    852 FORMAT( /, 15X, 'ROOT LENGTH, M/SQ.M, BY LAYER', T102, 'TIME')
    WRITE (6,854) (PRTL(J),J=1,NJ), TIME
* WRITE (6,854)
    851 FORMAT(//, 35X, ' ROOT GROWTH RATE', 50 X, 'MATRIC POTENTIAL')
    WRITE (6,854) (RTGRO(J),J=1,NJ), (POTM(J), J=1,2)
    127 CONTINUE
*
* ** ROOT DEATH IN EACH LAYER **
*
SUMRD = 0.0
DO 649 I = 1, NNJ
RTDTH(I) =PRTL(I) * DTHFAC * TMPFCR
* ROOT DEATH, AS METERS/SECOND LOST FROM EACH LAYER
    SUMRD = SUMRD + RTDTH(I)
    6 4 9 \text { CONTINUE}
    RTDTH(NJ) = 0.
*
    SUMRTD = 0.0
    DO 651 I = 1, NNJ
    IF (SUMRD.EQ.0.) GO TO 651
    RTDTH(I) = RTDTH(I) * ROOTDY/SUMRD * LNGFAC
* SCALES ACTUAL DEATH RATE TO TOTAL AGGREGATE REQUIRED FOR C-BALANCE
    SUMRTD = SUMRTD + RTDTH(I)
* TOTAL FOR PLANT, AS METERS/SQ. METER/SECOND
    651 CONTINUE
*
    IF (YY .GT. 0.1) GO TO 752
    IF (TIME.GT.300) GO TO 652
    752 CONTINUE
* WRITE (6,859)
    859 FORMAT(/, 35X, 'ROOT DEATH RATE')
* WRITE (6,854) (RTDTH(J),J=1,NJ)
    6 5 2 \text { CONTINUE}
* *
* ** SUMMARY OF GROWTH AND DEATH IN EACH LAYER **
*
        DO 653 I = 1,NNJ
        NETGRO(I) = RTGRO(I) - RTDTH(I)
        IF ( ROOTVL(I) .GT. POROS(I) * TCOM(I)) NETGRO(I) = 0
        NETWTG(I) = NETGRO(I) / LNGFAC
        NETVLG(I) = NETWTG(I) * 100 / ( RTDWPC * 1000.)
    6 5 3 \text { CONTINUE}
    NETGRO(NJ) = 0.
    NETWTG(NJ) = 0.
    NETVLG(NJ) = 0.
* NET CHANGE IN ROOT LENGTH, AS METERS/SECOND CHANGE IN EACH LAYER.
            IF (YY .GT. 1.0) GO TO 753
            IF (TIME.GT.300) GO TO 654
    753 CONTINUE
* WRITE (6,856)
    856 FORMAT( 35X, 'NET GROWTH')
* WRITE (6,854) (NETGRO(J), J=1,NJ)
```

```
* WRITE(6,857)
    857 FORMAT(/, 50X, 'ITERATION TO FIND POTCR', /)
    654 CONTINUE
*
    PRTL = INTGRL(IPRTL,NETGRO,10)
    ROOTWT = INTGRL(IRTWT,NETWTG,10)
    ROOTVL = INTGRL(IRTVL,NETVLG,10)
* PARTIAL ROOT LENGTH, IN EACH SOIL LAYER -- SUM OF GROWTH LESS DEATH
*ENDPRO
*
* ** ROOT SYSTEM RESISTANCE AND WATER UPTAKE ***
*
NOSORT
**PROCEDURE RSSL, PTOTL, RSRT, AAAA, BBBB, CCCC = PROC4(COND,SUMRG,DDDD)
        DO 102 I = 1,NNJ
        RSSL(I) = 1./(B*COND(I)*(PRTL(I)+NOT(PRTL(I))*1.0E-10))
*PARAM B = (1.0E-04,1.0E-03,1.0E-02,1.0E-01,1.0)
PARAM B = 1.0E-02
*PARAM B = 1.0E-04
* CONSTANT, RELATING ROOT CONDUCTIVITY TO ROOT LENGTH, AFTER GARDNER.
    PTOTL(I) = POTH(I)
* NOTE THAT PTOTL IS THE SAME AS HYDRAULIC POTENTIAL IN THIS VERSION
PARAM URRS = 1.00E11
* UNITS FOR RADIAL RESISTANCE
PARAM UARS = 1.00E11
* UNITS FOR AXIAL RESISTANCE (IN THE XYLEM)
    RRS(I) = URRS / (PRTL(I) + NOT(PRTL(I))*1.0E-10)
* RADIAL RESISTANCE TO WATER FLOW IN THE ROOT
    ARS(I) = UARS * DEPTH(I) / (PRTL(I) + NOT(PRTL(I))*1.0E-10)
* aXIAL RESISTANCE -- ALONG THE XYLEM TRANSPORT SYSTEM
    RSRT(I) = RRS(I) + ARS(I)
* COMBINED AXIAL AND CONDUCTIVE RESISTANCE OF ROOTS IN THIS LAYER
    102 CONTINUE
**ENDPRO
*
*
* ** CALCULATION OF POTCR AND PARTITIONING OF ROOT WATER UPTAKE
* CUMREM = INTGRL(0.0,SUMR)
* CUMULATIVE WATER REMOVAL (BY ROOT SYSTEm) FROM ALL SOIL LAYERS
*
**PROCEDURE SUMR,DIFF,DIF,RTEX,POTCR,POTRT,AAAAA,BBBBB = ...
* PROC5(POTH, TRANSP, RUN, RSRT, CCCCC, DDDDD)
*
        COUNT = 0.0
* FLPFLP = -FLPFLP
    115 CONTINUE
        COUNT = COUNT + 1.0
        IF ( COUNT .LT. 100.0 ) GO TO 116
    * WRITE (6,666) TRANSP, SUMR, DIF, POTCR, COUNT, TIME
    666 FORMAT ( ' T S D P C ', 7E15.5 )
                GO TO 165
    * IN CASE THE LOOP DOES NOT CONVERGE In 100 TRIES, GO AHEAD ANYWAY
    116 CONTINUE
```

```
*
    SUMR = 0.0
    DO 150 J = l,NNJ
    I = J
    IF ( FLPFLP .EQ. l.0 ) I = NJ - J + 1
    RTEX(I) = AMAX1(0.0 ,(POTH(I) - POTCR) / (RSSL(I) + RSRT(I) ) )
* ROOT EXTRACTION, M/SECOND
    IF (RUNS.GT.02) GO TO 117
    IF (COUNT.GT.5) GO TO 117
* WRITE(6,854) J, I, POTH(I), POTCR, RSSL(I), RSRT(I), RTEX(I), ...
* SUMR, TRANSP, DIFF, DIF, COUNT
    1 1 7 \text { CONTINUE}
    SUMR = SUMR + RTEX(I)
* SUM OF Water removals by Roots in all Layers
    150 CONTINUE
        RTEX(NJ) =0.
        RTEX(NJJ) =0.
        DIFF = TRANSP - SUMR
* IF (SUMR .LT. TRANSP) RTEX(NJ) = AMAXI(RTEX(NJ),DIFF)
*
* FOR EACH LAYER, WATER EXTRACTION IS ASSUMED ON THE BASIS OF CURRENT
* VALUE FOR CANOPY POTENTIAL. ITERATION WILL CONTINUE UNTIL EQUAL.
        DIF = (SUMR - TRANSP) / TRANSP
        IF (COUNT.GT.l00.0) GO TO 165
        IF(RUNS.GT.2) GO TO 118
        WRITE(6,754)
    754 FORMAT(4X, 'DIF', 7X, 'SUMR', 5X, 'DIFF', 4X, 'POTCR')
        INSERTS HEADERS BETWEEN SUCCESSIVE PASSES IN ITERATION LOOP
            WRITE(6,854) DIF, SUMR, DIFF, POTCR
            WRITE(6, 860)
            WRITE(6,858)
    858 FORMAT(9X,'J',9X,'I',3X,'POTH',5X,'POTCR',7X,'RSSL',6X,'RSRT')
    860 FORMAT(T65,'RTEX',6X,'SUMR',5X,'TRANSP',6X,'DIFF',6X,'DIF')
    118 CONTINUE
            IF ( ABS(DIF) .LE. ERROR ) GO TO 165
* ADJUSTMENT OF CANOPY WATER POTENTIAL UP OR DOWN AS NEEDED TO BALANCE.
    160 POTCR = AMINl((POTCR - DIF*POTCR*CF),MAXPOT)
PARAM MAXPOT = -2.0
* MAXIMUM ALLOWABLE CANOPY POTENTIAL, (-2 METERS, OR -0.2 BARS)
            GO TO 115
*
    165 CONTINUE
            DO 170 I = 1,NNJ
            POTRT(I) = POTCR + RTEX(I) * RSRT(I)
    170 CONTINUE
**ENDPRO
*
* ** SUMMARY OF WATER MOVEMENT AND EVAPORATIVE LOSSES
*
        CRTEX = INTGRL ( 0.0 , RTEX ,11)
        CUMULATIVE ROOT EXTRACTION
        EVAP = AMIN1(-FLW(1), SLEVAP)
```

```
* EVAPORATION FROM SOIL SURFACE - LIMITED BY AVAILABILITY OF WATER
* (COMING FROM DEEPER SOIL LAYERS) OR BY THERMAL INSOLATION AT SURFACE
        CEVAP = INTGRL(0.0, EVAP)
* CUMULATIVE EVAPORATION FROM SOIL SURFACE
        DRAIN = INTGRL (0.,DRAING)
* INTERNAL DRAINAGE, AS WATER PASSES THE BOTTOM OF THE LOWEST LAYER
        FLWNJN = - AMIN1(0.0,FLW(NJJ))
        CAPRIS = INTGRL (0.,FLWNJN)
* CAPILLARY RISE, PAST THE BOTTOM LAYER
        CTRAN = INTGRL (0.,TRANSP)
* CUMULATIVE TRANSPIRATION, AS M/SQUARE METER
*
*
*
        IF (KEEP.NE.1) GO TO 314
* WRITE(11,313) HOURS,RADIAT,TEMP,SHOOTW,ROOTW,PHOTSN,WATRST
    313 FORMAT(5F8.3,G10.2,F8.3)
    314 CONTINUE
        RUNS = RUNS + 1
*
************* TERMINALSEGMENT **************
TERMINAL
*
PRINT DAY,HOUR, PHOTSN, POTCR, SOLCHO, SHOOTW, ROOTW,...
    ROOTW, CTRAN, CEVAP, DELT
*
    ZYY = DEBUG(01,TIME)
OUTPUT DAY,RADIAT,RAIN
LABEL RADIATION AND RAINFALL
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=05.0
OUTPUT DAY,TEMP,STEMP
LABEL AIR AND SOIL TEMPERATURE
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=05.0,GROUP=2
OUTPUT DAY,SHOOTW,ROOTW,DRYWT
LABEL DRY WEIGHT OF SHOOT AND ROOT (KG/M2)
LABEL
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=04.0,GROUP
OUTPUT DAY,LAI,ROOTL
LABEL LEAF AREA INDEX AND ROOT GROWTH
LABEL
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=04.0
OUTPUT DAY,FRAC(0.0,1.0)
LABEL BIOMASS PARTITIONING
LABEL
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=04.0
OUTPUT DAY,PHOTSN
LABEL PHOTOSYNTHESIS (KG/M2/SEC)
LABEL
PAGE XYPLOT, MERGE,HEIGHT= 3.,WIDTH=04.0
```

```
OUTPUT DAY,POTCR
LABEL CANOPY WATER POTENTIAL
LABEL
PAGE XYPLOT, MERGE,HEIGHT= 3.,WIDTH=04.0
OUTPUT DAY,TOPGRO, TOTRG, SHOOTD, ROOTDY
LABEL TISSUE GROWTH AND DEATH (KG/M2/S)
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=05.0,GROUP=4
OUTPUT DAY,SHMRES, SHGRES, RTMRES, RTGRES
LABEL COMPONENTS OF RESPIRATION ( KG/M2 )
LABEL
LABEL MAINTENANCE AND GROWTH OF SHOOT AND ROOT
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=04.0,GROUP=4
OUTPUT DAY,NETGRO(1-8)
LABEL NET INCREASE IN ROOT LENGTH (M/M2/S)
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=04.0,GROUP
OUTPUT DAY,TRANSP,EVAP
LABEL TRANSPIRATION AND EVAPORATION (M/S)
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=04.0,GROUP
OUTPUT DAY,CTRAN,CEVAP
LABEL CUMULATIVE WATER UPTAKE AND EVAPOTRANSPIRATION (M)
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=04.0,GROUP
OUTPUT DAY,NFLW(1-8)
LABEL NET FLOW OF WATER (M3/M2/S)
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=04.,GROUP
OUTPUT DAY,RTEX(1-8)
LABEL ROOT EXTRACTION (M3/M3/SEC)
LABEL
PAGE XYPLOT, MERGE,HEIGHT=3.,WIDTH=04.,GROUP
OUTPUT DAY,POTM(1-8)
LABEL SOIL MATRIC POTENTIAL
LABEL
PAGE XYPLOT,MERGE,HEIGHT=3.,WIDTH=04,GROUP
OUTPUT DAY,THETA(1-8)
LABEL SOIL WATER CONTENT
LABEL
PAGE XYPLOT,MERGE,HEIGHT=3.,WIDTH=04,GROUP
OUTPUT DAY,PRTL(1-8)
LABEL PARTIAL ROOT LENGTH (M/M2)
LABEL
PAGE XYPLOT,MERGE,HEIGHT=103.,WIDTH=04.,GROUP
*
END
STOP
ENDJOB
```


## APPENDIX B:

FORTRAN LISTING OF SIMULATION MODEL

```
C
C
C *** WATER UPTAKE AND ROOT GROWTH IN A HOMOGENEOUS SOIL PROFILE
C
C SUBROUTINE UPDATE (SUPPLIED BY CSMP TRANSLATOR)
C (AS MODIFIED BY M. G. HUCK & G. HOOGENBOOM)
C VERSION 4.0 --- MAY 1985
C
C * * * * * * * * * * SYSTEM SEGMENT * * * * * * * * * * * * * * *
C
C SYSTEM SEGMENT OF MODEL
        INTEGER RUNS, MONTH, JDAY, DATE
        REAL*4 IMPULS,NOTT,IRFAC,IRMIN,IRQUAN,PULSIR,PULSSW,PULS1,INSW
        REAL*8 VOLW ( 20)
        REAL*8 PRTL ( 20),IPRTL(20),IRTWT(20),IRTVL(20),ROOTWT(20)
        REAL*8 CRTEX ( 20),ROOTVL(20)
        REAL*4 NFLW ( 20),IVOLW ( 20), POROS(20),BULKDS(20)
        REAL*4 NETGRO( 20),NETWTG(20),NETVLG(20)
        REAL*4 RTEX ( 20)
        REAL*4 TIME, ZZTIME, PRDEL,LSNHS,MINRTL,NU,MU
        EQUIVALENCE(ZZTIME,TIME )
C EQUIVALENCE(DFOVTX,DFCLTX,SUNTBX)
    REAL*8 SOLCHO, CUMRAD, DAYCUM, DRCI, DROI, DRADI,
    $ CSTMRS, CRTMRS, SHOOTW, POTCRD, ROOTW, CUMRAN, CUMPET,
    $ CUMREM, CEVAP, DRAIN, CAPRIS, CTRAN ,SNLS
    REAL*4 RSRT ( 20)
    REAL*4 DIST ( 20)
    REAL*4 THETA ( 20)
    REAL*4 RRS ( 20)
    REAL*4 ARS ( 20)
    REAL*4 FLW ( 20)
    REAL*4 COND ( 20)
    REAL*4 AVCOND( 20)
    REAL*4 POTRT ( 20)
    REAL*4 POTH ( 20)
    REAL*4 POTM ( 20)
    REAL*4 RSSL ( 20)
    REAL*4 Y ( 20)
    REAL*4 SCALE ( 20)
    REAL*4 BIRTH ( 20)
    REAL*4 EXTENS( 20)
    REAL*4 RTGRO ( 20)
    REAL*4 RTDTH (20)
    REAL*4 RRL(20)
    REAL*4 ITHETA(20)
    REAL*4 TCOM(20)
    REAL*4 MAXTEM
    REAL*4 MAXTMP
    REAL*4 MINTEM
```

```
        REAL*4 MINTMP
        REAL*4 MAXSTM
        REAL*4 MINSTM
        REAL*8 INTGRL, OLDVAL
        REAL*4 ICHO ,JULIAN, LFOV, LFCL, LOPOT, LAT
        1,ISHOOT,IROOT ,IPER ,LEAFTH,LNGFAC,MAXFOT,MAXPOT,MAXRAD,LAITBL
        1,IL ,IRTL ,LAI ,LAIFAC,MPANEV,MPOT, MXPHOT,LEAFW
```

C
REAL*4 SMAX (6), $\operatorname{SMIN}(6), \operatorname{SUNTBX}(10), \operatorname{DFCLTX}(10), \operatorname{DFOVTX}(10)$,
$1 \operatorname{DFOVTY}(10), \operatorname{DFCLTY}(10), \operatorname{SUNTBY}(10), \operatorname{SUTBX}(13), \operatorname{SUTBY}(13)$,
2FRACTX (5) , $\operatorname{FRACTY}(5), \operatorname{DTBLX}(6), \operatorname{DTBLY}(6), \operatorname{TRANX}(6), \operatorname{TRANY}(6)$,
3AVPETX (2) , AVPETY(2), LAITX(6), LAITY(6), TIMEX (400) , RADNY(400),
4MAXTMY (400) , MINTMY (400) , RAINY (400) , $\operatorname{PEVAPY}(400), \operatorname{MAXSTY}(400)$,
5MINSTY(400), BULKX (5) , BULKY (5)
DIMENSION PTOTL(20)
DIMENSION RK(20), DEPTH(20)
C
C TABLE DEFINITIONS:
DATA SUNTBX/ 0., 5., 15., 25., 35., 45., 55., 65.,
\$ 75., 90.1
DATA DFCLTX / 0., 5., 15., 25., 35., 45., 55., 65.,
\$ 75., 90./
DATA DFOVTX / 0., 5., 15., 25., 35., 45., 55., 65.,
\$ 75., 90.1
DATA DFOVTY / 0., 6., 26., 45., 64., 80., 94., 105.,
\$ 112., 116./
DATA DFCLTY / 0., 29., 42., 49., 56., 64., 68., 71.,
\$ 75., 77./
DATA SUNTBY / 0., 0., 88., 175., 262., 336., 402., 452.,
\$ 483., 504.1
C
C FUNCTION DEFINITIONS:
C FUNCTION SUTB $=(.025,20),.(.05,5),.(.075,3.0)$, ...
C $\quad(.10,1.7),(.15,0.6),(.20, .25), \quad$.
C (.25, .15) , (.30, . 10 )
C $\quad(.35, .05),(.40,0.01),(.45,0.0), \ldots$
C $\quad(.50,-1.00)$
DATA SUTBX $/ 0.00, .0674, .0940, .1119, .1263, .1363,0.1531, .1705, .2063$,
\$ $0.2461,0.36,0.42,0.50 /$
DATA SUTBY/60.,40.8,21.21,15.27,7.325,4.11,2.01,0.99,0.425,
\$ 0.264,0.0,0.0,0.0/
C FUNCTION FRACTB $=-500 ., .05,-200 ., .25,-050 ., .70,-10 ., .95, \ldots$
C 100.,. 95
DATA FRACTX/-500., -200., -50., -05., +100. /
DATA FRACTY/ .05, .20, .65, .90, . 90
C FUNCTION DTBL $=0.0,0.0,2.0,0.03,5.0,0.33,07.0,0.97,10 ., 100$.
DATA DTBLX $/ 0.0,2.0,5.0,7.0,10.0,25 . /$
DATA DTBLY/0.0, .03, 0.33, $0.97,1.0,1.0 /$
C FUNCTION TRNTBL $=-500 ., .05,-200 ., .05,-100 ., 0.95,0 ., 1.0,100 ., 1.0$
DATA TRANX $/-500 .,-245 .,-163 .,-112 ., 0.001,+100 . /$
DATA TRANY/ $0.05,0.05,0.50,0.95,1.00,1.00$ /
C FUNCTION LAITBL $=0 ., 0 ., 3.0,0.5,6.0,0.9,10.0,0.95$
DATA LAITX/ $0.0,2.0,4.0,6.0,10.0,25.0 /$
DATA LAITY/ $0.0,0.5,0.8,0.9,0.95,0.95$ /

```
            DATA BULKX/0.0,0.5,1.0,1.5,2.0/
            DATA BULKY/1.52,1.52,1.52,1.52,1.52/
            DATA RADNY/400*1.0/
            DATA MAXTMY/400*40./, MINTMY/400*10./
            DATA RAINY/400%0./, PEVAPY/400*0./
            DATA MAXSTY/400*30./, MINSTY/ 400%10./
C
C ********* * INITIAL SEGMENT ****************
C INITIAL SEGMENT OF MODEL
C
    RUNS=0
    KEEP = 1
    TIME = 0.0D00
    HOURS=TIME / 3600.0
    DAY=HOURS / 24.00
    PI=3.14159
    RAD=PI / 180.
    READ (8,*) FINTIM, OUTDEL, PRDEL, DELT, BGNDAY
    READ (8,*) IPER, ISHOOT, IROOT, LNGFAC, NJ,RTDWPC
    NJJ = NJ + 1
    NNJ = NJ - 1
    READ (8,*) (ITHETA(I), I=1,NJJ)
    READ (8,*) (RRL(I), I=1,NJ)
    READ (8,*) (TCOM (I),I=1,NJJ)
    READ (8,*) LOPOT, HIPOT
    C FOR LINEAR INTERPOLATION OF POTCR, WHEN THIS IS USED.
        READ (8,*) DTRDEM, SATCON, ZLAM, PARTDS,THTAIR,STHETA,ALPHA,NU
        READ (8,*) REFT, REFTS, RSPFAC, MXPHOT, DKPHOT, EFF
        READ (8,*) CONVRT, DELAY, FRG, AGFAC, LEAFTH, STWTR
        READ (8,*) GROFAC, DTHFAC, PB, BRMIN, EXTMIN, MINRTL
        READ ( 8,*) BR, EXTNRT, AA, BB, B, DEPTHG
        READ (8,*) URRS, UARS, MAXPOT, OUTF
        READ (8,*) POTCR, LSNHS, DRCI, DROI, DRADI
        READ (8,*) CF, ERROR, LAT
    C
        DO 79 I = 1,400
        TIMEX(I) = I
        79 CONTINUE
    C
C
        CSLT=COS(RAD*LAT)
        SNLT=SIN(RAD*LAT)
        PHTCAR=30./44.
    C MOLECULAR WEIGHT/VOLUME RATIO FOR CO2
C
        READ(12,91,END=193)RADN,MAXTEM,MINTEM,CMRAIN,PEVAP,MAXSTM,MINSTM,
        $ SIMDAY
        91 FORMAT(F4.0,F5.1,F6.1,F6.2,F7.3,F3.0,F3.0,
            $ 4lx,F3.0)
C READ(12,91,END=193)SIMDAY, RADN,MAXTEM,MINTEM, CMRAIN,PEVAP,
C $ MAXSTM, MINSTM
C 91 FORMAT(8F8.2,2I6)
    START = SIMDAY
    REWIND }1
```

```
        WRITE(6,92)SIMDAY,RADN,MAXTEM,MINTEM, CMRAIN, PEVAP,MAXSTM,
    $ MINSTM
C
    WRITE(19,1853)
    WRITE(6,1853)
1853 FORMAT(/,' INITIATE ',/,'SIMDAY',3X,'RADN',3X,' MAXTEM',
    $ ' MINTEM', ' CMRAIN', ' PANVAP', ' MAXSTM',
    $ ' MINSTM', ' MONTH', ' DATE', / )
    IF(SIMDAY.GT.400)GO TO 193
C
C
        DO 01 KOUNT=1,365
C READ(12,91,END=193)SIMDAY, RADN,MAXTEM,MINTEM,CMRAIN,PEVAP,
C $ MAXSTM, MINSTM, MONTH, DATE
        READ(12,91,END=193,ERR=193) RADN,MAXTEM,MINTEM,CMRAIN,PEVAP,
        $ MAXSTM,MINSTM,SIMDAY
        JDAY = SIMDAY
        CALL MTIME(MONTH,DATE,JDAY)
C MAXSTM = MINSTM + 0.75 * (MAXTEM - MINTEM)
C (NOTE THAT THIS APPROXIMATION IS NEEDED ONLY FOR SOUTHERN HEMISPHERE)
        IF(SIMDAY.GT.400)GO TO 101
92 FORMAT(F6.1,E10.2,6F07.2,2I5)
101 CONTINUE
        K = SIMDAY
        TIMEX(K) = SIMDAY
        RADNY(K) = RADN * 3600.
C CONVERTS FROM LY/SQ. CM. INTO JOULES/SQ. METER
        MAXTMY (K) = ( MAXTEM - 32. ) * 5./9.
        MINTMY(K) = ( MINTEM - 32. ) * 5./9.
C CONVERTS FROM DEGREES FAHRENHEIT INTO DEGREES C.
        RAINY(K) = CMRAIN * 2.54
        PEVAPY(K) = PEVAP * 2.54
C CONVERTS INCHES OF RAINFALL OR EVAPORATION INTO CENTIMETERS.
        MAXSTY(K) = ( MAXSTM - 32. ) * 5./9.
        MINSTY(K) = ( MINSTM - 32. ) * 5./9.
WRITE(6,92)SIMDAY,RADNY(K),MAXTMY(K),MINTMY(K),RAINY(K),PEVAPY(K),
        $ MAXSTY(K),MINSTY(K),MONTH,DATE
WRITE(19,92)SIMDAY,RADNY(K),MAXTMY(K),MINTMY(K),RAINY(K),PEVAPY(K)
        $ , MAXSTY(K),MINSTY(K),MONTH,DATE
        O1 CONTINUE
C
    193 CONTINUE
        KK = START
        LL = SIMDAY
C
        KKK = KK + 10
        DO 307 K = 170,200
    307 CONTINUE
        JDAY=DAY+BGNDAY
C
        SHOOTW = ISHOOT
        POTCRD = 10.
        POTCRE = POTCRD
        ROOTW = IROOT
```

```
    DRYWT = SHOOTW + ROOTW
    STEMW = STWTR * SHOOTW
    LEAFW = SHOOTW - STEMW
    ICHO=(ISHOOT+IROOT)*IPER/(1.-IPER)
    SOLCHO = ICHO
    IRTL=ROOTW*LNGFAC
    LAI=LEAFW*LEAFTH
    ETA=2.0+3.0%ZLAM
    C
    DEPTH(1)=.5*(TCOM(1))
    DIST(1)=DEPTH(1)
    IVOLW(1)=ITHETA(1)*TCOM(1)
C
    DO 20 I=2,NJJ
    DIST(I)=.5*(TCOM(I-1)+TCOM(I))
    DEPTH(I)=DEPTH(I-1)+DIST(I)
    IVOLW(I)=ITHETA(I)*TCOM(I)
    VOLW(I) = ITHETA(I) * TCOM(I)
    THETA(I) = VOLW(I)/TCOM(I)
    BULKDS(I) = AFGEN(BULKX,BULKY,DEPTH(I))
    POROS(I) = 1 - (BULKDS(I) / PARTDS)
    CONTINUE
    POROS(1)= POROS(2)
    C
    DO 30 I=1,NJ
    DRAING = (AMAX1(0.0,THETA(NJJ)-STHETA))*TCOM(NJJ)/DELT
    THETA(I) = AMIN1(ITHETA(I),STHETS)
    POTM(I )=-AFGEN(SUTBX,SUTBY,THETA(I ))
    C POTM(I) = -0.01* EXP(-37.31* THETA(I) + 16.97)
    C (CHOOSE LOOKUP TABLE OR FUNCTION, DEPENDING ON DATA AVAILABLE)
        POTH(I)=POTM(I )-DEPTH(I)
    IPRTL(I)=IRTL*RRL(I)
    IRTWT(I) = IPRTL(I)/LNGFAC
    IRTVL(I) = IRTWT(I)*100./(RTDWPC*1000)
    RRS(I)=URRS/ (IPRTL(I) + NOTT(IPRTL(I))*1.0E-10)
    ARS(I)=UARS*DEPTH(I)/ (IPRTL(I) + NOTT(IPRTL(I))*1.0E-10)
    RSRT(I)=RRS(I)+ARS(I)
    CONTINUE
    DO 15 I=1,NJJ
    RTEX(I) = 0.0
    NFLW(I) = 0.0
15 FLW(I)=0.0
    RISE = 4.8
    PLSNHS = 0.0
    TOPGRO = 0.0
    TOTRG = 0.0
    GROWTH = TOPGRO + TOTRG
    SHOOTD = 0.
    ROOTDY = 0.
    CUMRAD = 0.00
    DAYCUM = 0.00
    DRCP = 3.5E+07
    DROP = 6.6E+06
    DRCI = DRCP
```

DROI $=$ DROP
DRADI $=1.0 \mathrm{E}-10$
DRADZ = DRADI
DROZ $=$ DROI
DRCZ $=$ DRCI
RAINZ $=0.00$
DAYRAI $=0.00$
DRADI $=0.00$
PULS $=0.00$
PEVV $=0.00$
CSTMRS $=0.0$
CRTMRS $=0.0$
CUMRAN $=0.00$
CUMPET $=0.0 \mathrm{DO}$
DO $37 \mathrm{I}=1, \mathrm{NJ}$
$\operatorname{VOLW}(I)=\operatorname{IVOLW}(I)$
$\operatorname{PRTL}(I)=I P R T L(I)$
ROOTWT(I) $=$ IRTWT (I)
ROOTVL(I) $=$ IRTVL (I)
$\operatorname{CRTEX}(I)=0.0$
$\operatorname{RTEX}(\mathrm{I})=0.0$
$37 \operatorname{NETGRO}(\mathrm{I})=0.0$
CUMREM $=0.0$
CEVAP $=0.0 \mathrm{DO}$
DRAIN $=0.0$
CAPRIS $=0.0$
CTRAN $=0.0$
SUMR $=0.0$
COUNT $=0.0$
DTOT $=0.0$
DTOTI $=0.0$
$\mathrm{DTOTZ}=0.0$
RATE $=0.0$
C
TIME $=0.0 \mathrm{D} 00$
HOUR $=0.0$
$\mathrm{XXX}=0.0000$
$Y Y=0.0$
C
WRITE (1,876)
876 FORMAT(1X, 'HOURS', 3X, 'POTH(1)', 2X, 'POTH(2) ETC. --->')
WRITE $(2,877)$

WRITE $(3,878)$
878 FORMAT(2X, 'HOURS', 5X, 'HOUR', 4X, 'POTCRE', 4X, 'POTCR', \$ 6X, 'SOLCHO', 5X, 'SHOOTW', 4X, 'ROOTW', 5X, 'CTRAN', 5X, \$ 'CEVAP', 4X, 'JULIAN')
WRITE $(4,879)$
879 FORMAT(3X, 'HOURS', 3X, 'PHOTSN', 4X, 'GROWTH', 5X, 'RESP',
\$ 6X, 'ZZ1022', 4X,'SUMR', 6X,
\$ 'EVAP', 5X, 'TRANSD')
WRITE (9,880)
880 FORMAT(2X, 'HOURS', 5X, 'RADN', 6X, 'TEMP', 7X, 'PET', \$ 7X, 'RSSL(3)', 3X, 'RSRT(3)', 3X, 'COND(3)', 5X, 'RESP', 5X,

```
        $ 'SUMRTG', 4X, 'SUMRTD')
            WRITE(10,881)
    881 FORMAT(2X, 'HOURS RTEX(1) RTEX(2) ETC. ---> ')
        WRITE(11,882)
    882 FORMAT(2X, 'HOURS', 6X, 'LFOV', 6x, 'DTR', 6x, 'DTRR', 6X,
        $ 'LFCL', 6X, 'CRO', 7X, 'CRC', 7X, 'RANGE', 6X, 'AVAT', 5X,
        $ 'STEMP')
            WRITE(13,883)
    883 FORMAT(2X, 'HOURS', 6X, 'MONTH', 4X, 'DATE', 6X, 'HOUR', 6X,
        $ 'RAIN', 6X, 'ROOTDY', 4X, 'LAI', 7X, 'FLW(8)', 6X,' TEMP',
        $ 5X,'STEMP')
            WRITE(14,884)
    884 FORMAT(2X, 'HOURS', 6X, 'MONTH', 4X, 'DATE', 6X, 'HOUR', 6X,
        $ 'DRC ', 6X, 'DRCP ', 4X, 'DRO', 7X, 'DROP ', 6x, 'LFCL',
        $ 5X, 'RADCAL')
            WRITE(15,885)
    885 FORMAT(2X, 'HOURS', 6X, 'MONTH', 4X, 'DATE', 6X, 'HOUR', 6X,
        $ 'WATRST', 4X, 'PHOTC ', 4X, 'PHOTD', 5X, 'PHOTSN', 6X, 'LAI ',
        $ 5x, 'LFCL ')
        WRITE (6,1856)
    1856 FORMAT(/,' INITIATION NOW COMPLETE. ENTER DYNAMIC LOOP',//)
C
C * * * * * * * * * * DYNAMIC SEGMENT * * * * * * * * * * * * * * *
C DYNAMIC SEGMENT OF MODEL
C
C
C
    6 0 0 1 ~ C O N T I N U E ~
        JULIAN=BGNDAY+TIME/86400.
        JDAY=JULIAN
        CALL MTIME(MONTH,DATE,JDAY)
        T=MONTH
        TT=T
        MTH=MONTH-0.5+((DAY/30))
        RUN=RUNS
        HOURS=TIME/3600.0
        HOUR=AMOD(HOURS,24.0)
        DAY=HOURS/24.00
        YY = AMOD(HOURS,OUTDEL)
        XXX = AMOD(TIME,PRDEL)
        IF (TIME.GT.1.0D15) GO TO 6002
C IF (YY .GT.0.01 ) GO TO 6002
    6 0 0 2 ~ C O N T I N U E ~
C
C
    IF (TIME.GT.fINTIM) GO TO 99
    IF (HOURS.GT.1200.) GO TO 99
    IF (POTCR.LT.-476.) GO TO 99
    IF (SOLCHO.LT.+1.0E-07) GO TO 99
C
C
    DEC=-23.4*COS(2.*PI*(JULIAN+10.)/365.)
C CHANGE TO -23.4 WHEN WORKING WITH DATA FROM NORTHERN HEMISPHERE
C DEC=+23.4*COS(2.*PI*(JULIAN+10.)/365.)
```

```
C (+10 IS TIME BETWEEN DEC 21 AND DEC 31--FOR SIDEREAL YEAR)
C
    SNDC=SIN(RAD*DEC)
    CSDC=COS(RAD*DEC)
    SNHSS=SNLT*SNDC+CSLT*CSDC*COS(PI*(HOUR+12.)/12.)
C SINE OF SUN HEIGHT(INCLUDING NEGATIVE VALUES)
    SNLS = SNHSS - LSNHS
    RISE1= (AND(SNHSS,-LSNHS))-0.5
    RISE2= HOUR-SNHSS*DELT/((NOTT(SNLS)+SNLS)*3600.)
    RISE = ZHOLD(RISE,RISE1,RISE2)
C TIME OF SUNRISE
    LSNHS =SNHSS
C SINE HEIGHT OF SUN ON PREVIOUS DAY
C
    DTRR=AFGEN(TIMEX, RADNY,(JULIAN-0.0))
C DAILY TOTAL GLOBAL RADIATION(MEASURED, INTERPOLATED FROM DAY TO DAY.
    DTR=RADNY(JDAY)
C DAILY TOTAL RADIATION (FROM INPUT FILE--JOULE/METER2/DAY)
    SNHS=AMAXI(0.,SNHSS)
C SINE, HEIGHT OF SUN, NEGATIVE VALUES REMOVED
    HSUN=ATAN(SNHS/SQRT(1.-SNHS*SNHS))/RAD
C HEIGHT OF THE SUN, EXPRESSED IN DEGREES, ABOVE HORIZON
    SUNDCL=AFGEN(SUNTBX,SUNTBY, HSUN)
C SUNLIGHT, DIRECT, UNDER A CLEAR SKY.
        DIFCL=AFGEN(DFCLTX,DFCLTY,HSUN)
C DIFFUSE VISIBLE RADIATION UNDER A STANDARD CLEAR SKY
        CRC=(SUNDCL+DIFCL)*2.
C CURRENT RADIATION INTENSITY UNDER A CLEAR SKY (DIRECT + DIFFUSE)
        DIFOV=AFGEN(DFOVTX, DFOVTY,HSUN)
C DIFFUSE VISIBLE RADIATION UNDER A STANDARD OVERCAST
        DIFON=0.7*DIFOV
C DIFFUSE NEAR-INFRARED UNDER A STANDARD OVERCAST SKY
        CRO=DIFOV+DIFON
C CURRENT RADIATION UNDER AN OVERCAST SKY
    CALL DLYTOT(DROZ,DRO,DROI,CRO,TIME,DELT)
    CALL DLYTOT(DRCZ,DRC,DRCI,CRC,TIME,DELT)
    PULS = IMPULS(TIME,0.0,86400.)
    DRCP = ZHOLD(DRCP,PULS,DRC)
    DROP = ZHOLD(DROP,PULS,DRO)
    FCL=(DTR-DROP) /(AMAXl((DRCP-DROP),0.0001))
C FRACTION OF THE TIME THAT SKY IS CLEAR
        FOV=1.-FCL
C FRACION OF THE TIME THAT SKY IS OVERCAST
        LFOV=AMIN1(1.,FOV)
        LFOV=AMAX1(0.,LFOV)
        LFCL=1.-LFOV
C FRACTIONS FCL AND FOV RESTRAINED BETWEEN O AND 1 (IN CASE OF ERROR)
        RADCAL=LFCL*CRC+LFOV*CRO
C RADIATION, CALCULATED--INSTANTANEOUS RATE
    CUMRAD =INTGRL (CUMRAD,RADCAL,DELT)
C CUMULATIVE TOTAL RADIATION RECEIVED--COMPARE WITH INPUT VALUES.
        CALL DLYTOT(DRADZ,DRAD,DRADI,RADCAL,TIME,DELT)
C
C
```

```
        MAXTEM = AFGEN(TIMEX,MAXTMY,(JULIAN-(14./24.)))
        MINTEM = AFGEN(TIMEX,MINTMY,(JULIAN-(RISE/24.)))
C LINEAR INTERPOLATION FROM INPUT DATA-FILE
        RANGE = (MAXTEM - MINTEM) * 0.250
C GENERATING FACTOR -- MINIMUM AT 3 AM; MAXIMUM AT 3 PM
```

        AVAT \(=(\) MAXTEM + MINTEM) \(* 0.500\)
    C AVERAGE AIR TEMPERATURE
CALL WAVE (TEMP, JULIAN, HOUR, MINTEM, MAXTEM, RISE, PI)
C COMPUTED AIR TEMPERATURE, DEGREES C.
C
MAXSTM $=\operatorname{AFGEN}(T I M E X, \operatorname{MAXSTY},(\operatorname{JULIAN}-(14 .+4) / 24.)$.
MINSTM $=$ AFGEN(TIMEX,MINSTY,(JULIAN-(RISE+4.) $/ 24$.$) )$
C LINEAR INTERPOLATION FROM INPUT DATA-FILE
RANGES $=($ MAXSTM - MINSTM $) * 0.500$
C AMPLITUDE (RANGE) OF DAILY SOIL TEMPERATURE OSCILLATIONS
AVST $=($ MAXSTM + MINSTM $) * 0.500$
C AVERAGE SOIL TEMPERATURE, FROM DAILY MEASUREMENT DATA
C
CALL WAVE (STEMP, (JULIAN-0.16), (HOUR-4.) ,MINSTM,MAXSTM,RISE, PI)
C SOIL TEMPERATURE, AS DEGREES CELSIUS
C
C
TMPFCS $=10.0 * *(($ TEMP-REFT $) * 0.030103)$
TMPFCR $=10.0 * *((S T E M P-R E F T S) * 0.030103)$
C BIOLOGICAL Q-10 -- DOUBLING REACTION RATE AT EACH 10 DEGREE TEMP CHNG
C
C*
C** $* *$ ESTIMATION OF RADIATION INTENSITY $* *$
C*
C*
C* $* *$ PHOTOSYNTHETIC ACTIVITY $* *$
C*
LAI=LEAFW *LEAFTH
LAIFAC=AFGEN(LAITX, LAITY, LAI)
WATRST=AFGEN(TRANX, TRANY, POTCR)
C
RADCPH $=0.5 *$ CRC
RADOPH $=0.5 *$ CRO
C PHOTOSYNTHETIC ACTIVE RADIATION
SLLA $=$ AMIN1 (LAI, $2 *$ SNHS $)$
C SUNLIT LEAF AREA
DLLA $=$ LAI - SLLA
C TOTAL LEAF AREA IN THE SHADE
XOVC $=$ RADOPH $* E F F /($ MXPHOT $*$ LAI )
POVC $=$ XOVC $/($ XOVC +1.$)$
PHOTD $=$ LAI * MXPHOT * POVC
C MAXIMUM CANOPY PHOTOSYNTHESIS UNDER AN OVERCAST SKY
$X S=\operatorname{ALOG}(1+(0.45 * E F F * R A D C P H /(A M A X 1(S L L A, 0.0001) * M X P H O T)))$
$\mathrm{PS}=\mathrm{XS} /(1+\mathrm{XS})$
PHOTS $=$ SLLA * MXPHOT * PS

```
C MAXIMUM CANOPY PHOTOSYNTHESIS UNDER A CLEAR SKY FOR SUNLIT LEAFAREA
    XSH = ALOG( 1+(0.55 * EFF * RADCPH/(AMAX1(DLLA,0.0001)*MXPHOT)))
    PSH = XSH / ( 1 + XSH )
    PHOTSH = DLLA * MXPHOT * PSH
C MAXIMUM CANOPY PHOTOSYNTHESIS UNDER A CLEAR SKY FOR SHADED LEAFAREA
C
    PHOTC = PHOTS + PHOTSH
    IF ( LAI .GT. 3 ) GO TO 31
    IF ( RADCAL .LT. 1.0 ) GO TO 31
    FINT = ( 1. - EXP(-0.8*LAI))
    Cl = FINT * PHOTC
    C2 = LAI * MXPHOT
    01 = FINT * PHOTD
    O2 = C2
    IF ( C1 .GT. C2 ) GO TO 32
    C0 = C1
    C1 = C2
    C2 = C0
    32 CONTINUE
    PHOTC = C2 * ( 1. - EXP ( AMAX1(-50., ( - C1/C2))))
    IF ( O1 .GT. O2 ) GO TO 33
    00=01
    01=02
    02=00
    33 CONTINUE
    PHOTD = 02* ( 1. - EXP ( AMAX1(-50., ( -01/02))))
    31 CONTINUE
    PHOTSN = WATRST * ( PHOTC * LFCL + PHOTD * LFOV)
C PHOTOSYNTHETIC RATE (NET CARBON FIXATION, KG/SQUARE METER/SECOND
C
C*
C*
C*
    SHMRES=SHOOTW*TMPFCS*RSPFAC
    CSTMRS =INTGRL (CSTMRS ,SHMRES,DELT)
    SHGRES=TOPGRO*CONVRT
    RESPSH=SHMRES+SHGRES
    RTMRES=ROOTW*RSPFAC*TMPFCR
    CRTMRS =INTGRL (CRTMRS ,RTMRES,DELT)
    RTGRES=TOTRG*CONVRT
    RESPRT=RTMRES+RTGRES
    RESP=RESPSH+RESPRT
    ZZ1022 =(PHOTSN*PHTCAR-GROWTH-RESP)
    SOLCHO =INTGRL (SOLCHO ,ZZ1022,DELT)
    FRAC=AFGEN(FRACTX,FRACTY,POTCRE)
    TOPGRO =TMPFCS*GROFAC*SOLCHO*FRAC
    TOTRG=(1.0-FRAC)*TMPFCR*GROFAC*SOLCHO
    GROWTH=TOPGRO+TOTRG
    RESL=SOLCHO/(SOLCHO+ROOTW+SHOOTW)
C* RESERVE LEVEL, % FREE CARBOHYDRATE IN TISSUES
    IF (RESL.GT.0.75) GO TO 99
    SHOOTW =INTGRL(SHOOTW,(TOPGRO-SHOOTD),DELT)
    ROOTW =INTGRL(ROOTW,(TOTRG-ROOTDY),DELT)
    ROOTL = ROOTW * LNGFAC
```

```
    DRYWT = SHOOTW + ROOTW
    STEMW = STWTR * SHOOTW
    LEAFW = SHOOTW - STEMW
    DTHBGN=AFGEN(DTBLX, DTBLY, LAI)
    AGING=AGFAC*(DAY/30.)
    SHOOTD=SHOOTW*TMPFCS*DTHBGN*AGING
    ROOTDY=ROOTW/RESL*DTHFAC*TMPFCR
C
C
C
C
    PEVV=AFGEN(TIMEX, PEVAPY,JULIAN)*0.01
    PEVVV=PEVAPY(JDAY)*0.01
    PET=AMAX1(PEVV*0.01/86400.,RADCAL*PEVVV/(AMAX1 (0.01, DTR*1.0)))
    CUMPET =INTGRL (CUMPET ,PET ,DELT)
    TRANSD = PET * LAIFAC
C TRANSPIRATION DEMAND IN THE ABSENCE OF STOMATAL CLOSURE--USED IN
C ESTIMATING POTCR BY THE INTERPOLATION METHOD (BUT NOT ITERATIVE)
        TRANSP=WATRST*PET*LAIFAC
```



```
        IRFAC = 10.
        IRMIN = 10.2118* IRFAC / 100.
        PULSIR = IMPULS(TIME,0.0,1800.)
        IRQUAN = 000.0 * 1.0E-6
        PULSl = IRMIN+POTM(3)
        PULSSW = INSW(PULS1,IRQUAN,0.0)
        VOLW(1) = VOLW(1) + RAIN * DELT + PULSSW * PULSIR
C
        DO 1001 I = 1,NJJ
        BULKDS(I) = AFGEN(BULKX,BULKY,DEPTH(I))
        POROS(I) = 1 - (BULKDS(I) / PARTDS)
        THETA(I) = VOLW(I)/TCOM(I)
        DRAING = (AMAX1(0.0,THETA(NJJ)-STHETA))*TCOM(NJJ)/DELT
        THETA(I) = AMIN1(THETA(I),STHETA)
        VOLW(I) = THETA(I) * TCOM(I)
        POTM(I )=-AFGEN(SUTBX,SUTBY,THETA(I ) )
C POTM(I) = -0.01* EXP(-37.31* THETA(I) + 16.97)
C (CHOOSE LOOKUP TABLE OR FUNCTION, DEPENDING ON DATA AVAILABLE)
    POTH(I )=POTM(I )-DEPTH (I )
    CONTINUE
C
    DO 85 I=1,NJJ
    MPOT=-POTM(I )*100.0
        IF(MPOT.LE.0.0)GO TO }8
        MU = 1 - ( 1/ NU )
        AH = ALPHA * MPOT
        RK(I)=(1-(AH)**(NU-1)*(1+(AH)**NU)***(-MU))**2/
    $((1+(AH)**NU)***(MU/2))
C RELATIVE CONDUCTIVITY (AS A FRACTION OF SATURATED CONDUCTIVITY)
```

```
C RK(I)=(PB/MPOT)**ETA
    GO TO 87
    RK(I ) =1.0
    CONTINUE
    FORMAT(12G10.3)
    RK(I)=AMIN1(1.00,RK(I))
    COND(I)=RK(I)*SATCON
C COND(I) = 0.01* EXP(-5.69-2.059*ALOG(-POTM(I)*100.0))
C (CHOOSE BROOKS & COREY OR EXPONENTIAL, AS DATA INDICATES.)
85 CONTINUE
    DO 110 I=2,NJJ
    AVCOND(I) =.5*(COND(I-1)+COND(I ))
    FLW(I)=AVCOND(I)*(POTH(I-1)-POTH(I))/DIST(I)
110 CONTINUE
    FLW(NJJ+1) = DRAING
    NFLW(NJJ+1) = DRAING
    POTMAR = - AFGEN(SUTBX,SUTBY,THTAIR)
    IF(POTM(1).GT. POTMAR)FLW(1)=-SLEVAP
    IF(POTM(1).LE. POTMAR)FLW(1)=FLW(2)
    DO 120 I=1,NJJ
    NFLW(I)=FLW(I)-FLW(I+1)-RTEX(I)
120 CONTINUE
    DO 62 I = 1,NJJ
    VOLW(I) =INTGRL (VOLW(I) ,NFLW(I),DELT)
    6 2 \text { CONTINUE}
C*
C
C
C
    W=AMAX1(0.0,(POTM(2)-EXTMIN))
    DO 1010 I=1,NNJ
    X=AMAX1(0.0,(POTM(I)-BRMIN))
    XX=AMAX1(0.0,(POTM(I)-EXTMIN))
    BIRTH(I)=(BR*(1.0-EXP (-AA*X**BB)))/(((DEPTH(I)*DEPTHG))**1.)
    EXTENS(I)=(EXTNRT*(1.0-EXP(-AA*XX***BB)))/(((DEPTH(I)*DEPTHG))**1.)
    IF ( PRTL(I) .LT. MINRTL* TCOM(I)) EXTENS(I) = 0.
1010 CONTINUE
    RTGRO(1)=PRTL(1)*BIRTH(1) * (1.0 - FRAC) * TMPFCR
    SUMRG=RTGRO(1)
    DO 647 I=2,NNJ
    RTGRO(I)=(PRTL(I-1)*EXTENS(I-1)+PRTL(I)*BIRTH(I ) ) *
    $ (1.0 - FRAC) * TMPFCR
647 SUMRG=RTGRO(I )+SUMRG
    SUMRTG=0.0
    DO 648 I=1,NNJ
    IF(SUMRG.EQ.0.00)GO TO 648
    RTGRO(I )=RTGRO(I )*TOTRG/SUMRG*LNGFAC
    SUMRTG=SUMRTG+RTGRO(I)
648 CONTINUE
    IF(YY .GT.1.0)GO TO 127
    IF(TIME.GT.300)GO TO }12
751 CONTINUE
127 CONTINUE
    SUMRD=0.0
```

```
    DO 649 I=1,NNJ
    RTDTH(I)=PRTL(I )*DTHFAC*TMPFCR
649 SUMRD=SUMRD+RTDTH(I)
    SUMRTD=0.0
    DO 651 I=1,NNJ
    IF(SUMRD.EQ.0.)GO TO 651
    RTDTH(I)=RTDTH(I )*ROOTDY/SUMRD*LNGFAC
    SUMRTD=SUMRTD+RTDTH(I)
651 CONTINUE
    DO 653 I=1,NNJ
    NETGRO(I )=RTGRO(I )-RTDTH(I )
    IF ( ROOTVL(I) .GT. POROS(I)*TCOM(I)) NETGRO(I )=0.
    NETWTG(I) = NETGRO(I) / LNGFAC
    NETVLG(I) = NETWTG(I) * 100. / (RTDWPC*1000.)
6 5 3 ~ C O N T I N U E ~
    NETGRO(NJ) = 0.
    NETWTG(NJ) = 0.
    NETVLG(NJ) = 0.
    DO 63 I = 1,NNJ
    PRTL(I) =INTGRL (PRTL(I),NETGRO(I),DELT)
    ROOTWT(I) =INTGRL (ROOTWT(I),NETWTG(I),DELT)
    ROOTVL(I) =INTGRL (ROOTVL(I),NETVLG(I),DELT)
    63 CONTINUE
C
DO 102 I=1,NNJ
RSSL(I)=1./(B*COND(I)*(PRTL(I)+NOTT(PRTL(I))*1.0E-20))
PTOTL(I)=POTH(I)
RRS(I)=URRS / (PRTL (I )+NOTT(PRTL(I))*1.0E-10)
ARS(I)=UARS*DEPTH(I)/(PRTL(I )+NOTT(PRTL(I ) )*1.0E-20)
RSRT(I)=RRS(I)+ARS(I)
102 CONTINUE
C
    CUMREM =INTGRL (CUMREM ,SUMR ,DELT)
    COUNT=0.0
115 CONTINUE
    COUNT=COUNT+1.0
    IF(COUNT.LT.100.0)GO TO 116
    GO TO 165
116 CONTINUE
C
    SUMR=0.0
    DO 150 J=1,NNJ
    I=J
    RTEX(I)=AMAX1(0.0,(POTH(I)-POTCR)/(RSSL(I)+RSRT(I)))
    IF(RUNS.GT.02)GO TO 117
    IF(COUNT.GT.3)GO TO 117
117 CONTINUE
        SUMR=SUMR+RTEX(I)
    150 CONTINUE
C
DIFF=TRANSP-SUMR
DIF=(SUMR-TRANSP)/TRANSP
IF(COUNT.GT.100.0)GO TO 165
IF(RUNS.LT.099)GO TO 118
```

DOUBLP $=($ POTCR-POTCRD) $/$ DELAY
POTCRD = INTGRL(POTCRD,DOUBLP,DELT)
SINGLP $=$ POTCRD
POTCRE=AMIN1 (POTCR, SINGLP)
C SINGLP IS A REAL*4 REPRESENTATION OF POTCRD, FOR THE AMIN1 FUNCTION
DO $67 \mathrm{I}=1$, NNJ
CRTEX(I) =INTGRL (CRTEX(I) ,RTEX(I),DELT)
67 CONTINUE
C
EVAP=AMIN1 (-FLW(1), SLEVAP)
CEVAP =INTGRL (CEVAP ,EVAP ,DELT)
DRAIN =INTGRL(DRAIN,DRAING,DELT)
FLW8N=-AMIN1 (0.0,FLW (8))
CAPRIS =INTGRL (CAPRIS ,FLW8N ,DELT)
CTRAN =INTGRL (CTRAN ,TRANSP,DELT)
DRAING=FLW (8)
C
C IF (YY .GT.0.1)GO TO 1200
C OUTDEL $=$ OUTDEL + OUTDEL
C
1000 CONTINUE
1200 CONTINUE
C
TIME = TIME + DELT
RUNS $=$ RUNS +1
C
IF (XXX.GT.1) GO TO 6001
WRITE (1,276) HOURS, (POTH(I), I=1,09)
276 FORMAT (10E10.3)
WRITE (2,276) HOURS, (NFLW(I), $I=1,9)$
WRITE 3,276 ) HOURS, HOUR, POTCRE, POTCR, SOLCHO, SHOOTW, \$ ROOTW, CTRAN, CEVAP, JULIAN
WRITE (4,276) HOURS, PHOTSN, GROWTH, RESP, ZZ1022,
\$ SUMR, EVAP, TRANSD
WRITE(9,276) HOURS, RADCAL,TEMP, PET, RSSL(3), RSRT(3), COND(3), \$ RESP, SUMRTG, SUMRTD
WRITE ( 10,276 ) HOURS, (RTEX(I), $I=1,9)$
WRITE(11,276) HOURS, LFOV, DTR, DTRR, LFCL, CRO, CRC, RANGE, \$ AVAT, STEMP
277 FORMAT(1E10.3,2I10,7E10.3)
WRITE (13,277) HOURS, MONTH, DATE, HOUR, RAIN, ROOTDY, LAI, \$ FLW(8), TEMP, STEMP
WRITE (14,277) HOURS, MONTH, DATE, HOUR, DRC , DRCP , DRO,

```
        $ DROP , LFCL, RADCAL
        WRITE(15,277) HOURS, MONTH, DATE, HOUR,WATRST,PHOTC,PHOTD,
        $ PHOTSN,LAI,LFCL
        WRITE(16,276) HOURS, (PRTL(I),I=1,9)
        WRITE(17,276) HOURS, (ARS(I),I=1,9)
        WRITE(18,276) HOURS, (RRS(I),I=1,9)
        WRITE(6, 392) JULIAN,SHOOTW,ROOTW,LAI,ROOTL,PHOTSN,POTCR,TRANSP
        WRITE(20, 392) JULIAN,SHOOTW,ROOTW,LAI,ROOTL,PHOTSN,POTCR,TRANSP
    392 FORMAT(/' JULIAN=', F6.2,' SHOOTW=',F10.5,' ROOTW=',
        $F10.5,' LAI=', F8.3,/' ROOTL=', F10.3,' PHOTSN=',E10.2,' POTCR=',
        $ F10.2,' TRANSP=',E10.2)
        GO TO 6001
C
C
C
C***********TERMINAL SEGMENT ***************
C
C
C TERMINAL SEGMENT OF MODEL
    99 CONTINUE
        WRITE(6, 591) HOUR, MONTH, DATE
    591 FORMAT(//, ' FINISH CONDITION REACHED AT ', F4.1,
        $ ' HOURS ON', I4, ' /', I2)
            WRITE(6, 391) JULIAN,MAXRAD,RADN,LAI,WATRST,TIME,SOLCHO,POTCR
    391 FORMAT(//,' JULIAN = ',F8.4,' MAXRAD = ', F12.4,' ' RADN =',
        $F12.4,' LAI = ', F8.3,' WATRST = ', F10.3, //, 5X,
        $ ' TIME= ',F10.2,' SOLCHO = ',F10.7,' POTCR = ',F10.2,
        $ ' CUMREM',4X,' HOURS',5X,' XXX',6X,' YY')
        STOP
        END
C
        FUNCTION INSW(FIRST,SECOND,THIRD)
        REAL INSW
        INSW = THIRD
        IF (FIRST.LT.0.) INSW=SECOND
        RETURN
        END
C
        FUNCTION IMPULS(FIRST,SECOND,THIRD)
        REAL IMPULS
        IMPULS = 0.00000
        DO 10 I=1,10000
        COUNT = SECOND + I*THIRD
        IF (FIRST.LT.COUNT)GO TO 11
        IF (FIRST.EQ.COUNT)GO TO }1
    10 CONTINUE
    12 CONTINUE
        IMPULS = 1.
    11 CONTINUE
        RETURN
        END
C
        FUNCTION NOTT(INIT)
        REAL*8 INIT
```

```
    REAL*4 NOTT
    NOTT = 0.
    IF (INIT .LE. 0) NOTT = 1.
    RETURN
    END
    C
    C
    FUNCTION LIMIT(BOTTOM,TOP,START)
    REAL LIMIT
    LIMIT = START
    IF (START.LT.BOTTOM) LIMIT = BOTTOM
    IF (START.GT.TOP) LIMIT = TOP
    RETURN
    END
C
    FUNCTION AMOD(INPUT,INPUTD)
    REAL INPUT,INPUTD
    AMOD = INPUT
    DO 10 I=1,1000
    IF (AMOD .GT. INPUTD) AMOD = AMOD - INPUTD
    10 CONTINUE
    RETURN
    END
C
    FUNCTION ZHOLD(FIRST,INTEND,THIRD)
    REAL INTEND
    ZHOLD = FIRST
    IF ( INTEND .GT. 0.000001) ZHOLD=THIRD
    RETURN
    END
C
    FUNCTION INTGRL(OLDVAL,DERIV,DELT)
    REAL*8 INTGRL,OLDVAL
    INTGRL = OLDVAL + DERIV*DELT
    RETURN
    END
C
    FUNCTION AFGEN(XVAL, YVAL, ARG)
    REAL NEWX, NEWY, OLDX, OLDY
    DIMENSION XVAL(1), YVAL(1)
    OLDX = XVAL(1)
    OLDY = YVAL(1)
    DO 101 I = 2,400
    NEWX = XVAL(I)
    IF (ARG.LT.XVAL(I)) GO TO }10
    OLDX = NEWX
101 CONTINUE
102 CONTINUE
```

IF (OLDX.EQ.NEWX) OLDX = OLDX $-1.0 \mathrm{E}-10$
IF (OLDX.EQ.ARG) OLDX = OLDX - $1.0 \mathrm{E}-10$
NEWY $=$ YVAL (I)
OLDY $=$ YVAL $(\mathrm{I}-1)$
AFGEN $=$ OLDY $+(($ NEWY-OLDY $) /($ NEWX-OLDX $) *($ ARG-OLDX $))$
RETURN
END
C
SUBROUTINE MTIME (MONTH, DATE,JDAY)
INTEGER MONTH, DATE
INTEGER DAYS(13)
DATA DAYS / $0,31,59,90,120,151,181,212,243,273,304,334,365 /$
C CALENDAR--NUMBER OF DAYS AT END OF EACH MONTH
C (NOTE THAT FOR LEAP-YEARS, 1 MUST BE ADDED FOR FEB-DEC)
MONTH $=(\mathrm{JDAY} / 29)+1$
J=JDAY-DAYS (MONTH)
IF (J.GE.1) GO TO 775
MONTH=MONTH-1
J=JDAY-DAYS (MONTH)
775 CONTINUE
DATE $=\mathrm{J}$
RETURN
END
C
SUBROUTINE DLYTOT(DTOTZ,DTOT,DTOTI,RATE,TIME,DELT)
REAL IMP,IMPULS
REAL*8 INTGRL, DTOTI
DTOTI = INTGRL (DTOTI, RATE,DELT)
IMP =IMPULS (TIME, DELT, 86400.)
DUMMY $=$ DTOTI
DTOTZ $=$ ZHOLD (DTOTZ,IMP,DUMMY)
DTOT = DTOTI-DTOTZ
C
C THE ACCUMULATOR IS EMPTIED AFTER MIDNIGHT,
C SO CONTENTS ARE AVAILABLE FOR PRINTING.
RETURN
END
C
SUBROUTINE WAVE(TEMP, JULIAN, HOUR, MINT, MAXT, RISE, PI)
REAL MAXT,MINT,JULIAN, INSW
TIMI = HOUR - 14.
TIM2 $=$ HOUR +10 .
TIM $=$ INSW (TIM1, TIM2, TIM1)
C WRITE(6,11) TIM1,TIM2,TIM,HOUR
11 FORMAT(' TIM1 $=$ ',G10.2,'TMM2 $=^{\prime}, G 10.2,^{\prime}$ TIM $\left.=^{\prime}, G 10.2, ' H O U R=', G 9.2\right)$
VALAV $=0.5 *($ MAXT+MINT $)$
VALAMP $=0.5 *($ MAXT-MINT $)$
C $\operatorname{WRITE}(6,12)$ MAXT, MINT, VALAV,VALAMP
12 FORMAT(' MAXT $=$ ', G10.2,' MINT $=', G 10.2,^{\prime}$ VALAV=', G10.2,' VALAMP=',
\$ G10.2)
TEMPSR=VALAV-VALAMP*COS (PI*(HOUR-RISE) / (14.-RISE))
TEMPSS $=V A L A V+V A L A M P * \operatorname{COS}(P I * T I M /(10 .+R I S E))$
C

```
    13 FORMAT('TEMPSR=',G10.2,'TEMPSS=',G10.2,' VALAV=',G10.2,' VALAMP=',
        $ G10.2)
        AN1 = HOUR - RISE
        AN2 = 14. - HOUR
        AANNDD =-0.5 + AND(AN1,AN2)
        TEMP=INSW(AANNDD,TEMPSS,TEMPSR)
C WRITE(6,14) TEMPSR,TEMPSS,TEMP,AANNDD
14 FORMAT(' TEMPSR=',G10.2,' TEMPSS=',G10.2,' TEMP=',G10.2,' AND=',
        $ G10.2)
        RETURN
        END
```

```
            ACSL-LISTING OF SIMULATION MODEL (VERSION 1.5)
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| *****ADVANCED CONTINUOUS SIMULATION LANGUAGE***** '
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| *****ADVANCED CONTINUOUS SIMULATION LANGUAGE***** '
' *** VERSION 1.5 *** '
' *** VERSION 1.5 *** '
PROGRAM WATER UPTAKE AND ROOT GROWTH IN A HOMOGENEOUS SOIL PROFILE
PROGRAM WATER UPTAKE AND ROOT GROWTH IN A HOMOGENEOUS SOIL PROFILE
'CODED BY M.HUCK, D.HILLEL \& G.HOOGENBOOM, AUBURN UNIVERSITY -OCT.,1982'
'CODED BY M.HUCK, D.HILLEL \& G.HOOGENBOOM, AUBURN UNIVERSITY -OCT.,1982'
' (NOW INCLUDES SEPARATE GROWTH AND MAINTENANCE RESPIRATION FACTORS)
' (NOW INCLUDES SEPARATE GROWTH AND MAINTENANCE RESPIRATION FACTORS)
I
I
' AREA IS UNITY (M**2). UNITS SI (MKS).
' AREA IS UNITY (M**2). UNITS SI (MKS).
' ORGANIC MATTER PRODUCTION NORMALIZED TO 1 KG/M**2/YEAR
' ORGANIC MATTER PRODUCTION NORMALIZED TO 1 KG/M**2/YEAR
\prime WHICH IS 10 GM/M**2/DAY OR 0.01 MG/M**2/SEC, ON AVERAGE '
\prime WHICH IS 10 GM/M**2/DAY OR 0.01 MG/M**2/SEC, ON AVERAGE '
' FOLLOWING STATEMENT CHANGES INDEPENDENT VARIABLE TO TIME IN ACSL'
' FOLLOWING STATEMENT CHANGES INDEPENDENT VARIABLE TO TIME IN ACSL'
'CALL GSIZE(150.,11.0,1100)
'CALL GSIZE(150.,11.0,1100)
VARIABLE TIME = 0.0
VARIABLE TIME = 0.0
CINTERVAL CINT = 600.
CINTERVAL CINT = 600.
NSTEPS NSTEP = 1
NSTEPS NSTEP = 1
MINTERVAL MINT = 1.0
MINTERVAL MINT = 1.0
MAXTERVAL MAXT = 3600.
MAXTERVAL MAXT = 3600.
ALGORITHM IALG = 5
ALGORITHM IALG = 5
CONSTANT YY = 0.0
CONSTANT YY = 0.0
ARRAY CRTEX(10),RSRT(20), DIST(20), THETA(10), RRS(20), ARS(20)
ARRAY CRTEX(10),RSRT(20), DIST(20), THETA(10), RRS(20), ARS(20)
ARRAY VOLW(10),FLW(20), COND(20), AVCOND(20), POTRT(20),IVOLW(10)
ARRAY VOLW(10),FLW(20), COND(20), AVCOND(20), POTRT(20),IVOLW(10)
ARRAY POTH(20), POTM(20), RSSL(20), Y(20), SCAAL(20),IRTEX(10)
ARRAY POTH(20), POTM(20), RSSL(20), Y(20), SCAAL(20),IRTEX(10)
ARRAY NFLW(10),TCOM(10), RRL(10), SMIN(10), SMAX(10), ITHETA(10)
ARRAY NFLW(10),TCOM(10), RRL(10), SMIN(10), SMAX(10), ITHETA(10)
ARRAY PRTL(10),BIRTH(20), EXTENS(20), RTGRO(20), RTDTH(20)
ARRAY PRTL(10),BIRTH(20), EXTENS(20), RTGRO(20), RTDTH(20)
ARRAY IPRTL(10),NETGRO(10),RTEX(10),PTOTL(20)
ARRAY IPRTL(10),NETGRO(10),RTEX(10),PTOTL(20)
ARRAY LINE(101), RK(20), DEPTH(20)
ARRAY LINE(101), RK(20), DEPTH(20)
INTEGER J,NJ,NJJ,I,LINE,IX,IB,IFUN,RUNS,IL,KEEP
INTEGER J,NJ,NJJ,I,LINE,IX,IB,IFUN,RUNS,IL,KEEP
CONSTANT IX=1H*,IB=1H ,KEEP=1,LINE(1)=1HI
CONSTANT IX=1H*,IB=1H ,KEEP=1,LINE(1)=1HI
CONSTANT SMAX = . 35 , 4.50,.004 , 2.0,+0.3E-7, 5.0E2,0.,0.,0.,0.
CONSTANT SMAX = . 35 , 4.50,.004 , 2.0,+0.3E-7, 5.0E2,0.,0.,0.,0.
CONSTANT SMIN =.05 , -0.5 , 0.0 , -.1,-0.3E-7, 0.0,0.0,0.,0.,0.
CONSTANT SMIN =.05 , -0.5 , 0.0 , -.1,-0.3E-7, 0.0,0.0,0.,0.,0.
' SCALE FACTORS FOR VERTICAL GRADIENT PLOTS
' SCALE FACTORS FOR VERTICAL GRADIENT PLOTS
CONSTANT OUTF = 3.024E05
CONSTANT OUTF = 3.024E05
' OUTPUT FUNCTION FOR VERTICAL GRADIENT PLOTS MADE DURING EXECUTION --'
' OUTPUT FUNCTION FOR VERTICAL GRADIENT PLOTS MADE DURING EXECUTION --'
' --INITIAL FREQUENCY FOR VERTICAL GRADIENT PLOTS IS INCREMENTED LATER'
' --INITIAL FREQUENCY FOR VERTICAL GRADIENT PLOTS IS INCREMENTED LATER'
' SPECIFICATION OF CONVERGENCE CRITERIA FOR VARIABLE TIME-STEP INTGRLS'
' SPECIFICATION OF CONVERGENCE CRITERIA FOR VARIABLE TIME-STEP INTGRLS'
l
l
CONSTANT DAY = 0.0
CONSTANT DAY = 0.0
'
'
CONSTANT ERROR = 0.01
CONSTANT ERROR = 0.01
CONSTANT CF = 0.10
CONSTANT CF = 0.10
' CORRECTION FACTOR AND ERROR PARAMETERS FOR ITERATIVE LOOP BELOW '
' CORRECTION FACTOR AND ERROR PARAMETERS FOR ITERATIVE LOOP BELOW '
'
'
' A STANDARD MATHEMATICAL CONSTANT
' A STANDARD MATHEMATICAL CONSTANT
CONSTANT PI = 3.14
CONSTANT PI = 3.14
CONSTANT BGNDAY = 180.
CONSTANT BGNDAY = 180.
CONSTANT CLOCK = 0.
CONSTANT CLOCK = 0.
' JULIAN DATE AT BEGINNING OF SIMULATION RUN
' JULIAN DATE AT BEGINNING OF SIMULATION RUN
CONSTANT STEMP = 25.0
CONSTANT STEMP = 25.0
' TEMPERATURE OF THE SOIL, AS DEGREES C
' TEMPERATURE OF THE SOIL, AS DEGREES C
CONSTANT RANGE = 5.0

```
CONSTANT RANGE = 5.0
```

```
' RANGE BETWEEN AVERAGE (REFT) TEMPERATURE AND MINIMUM OR MAXIMUM
CONSTANT REFT = 25.0
'THE MEAN TEMPERATURE, ABOUT WHICH SIMULATED TEMPERATURE OSCILLATES
CONSTANT MAXRAD = 700.
' INCOMING RADIATION
CONSTANT MAXFOT = 3.00E-06
' MAXIMUM PHOTOSYNTHETIC RATE
!
!
1 ** INITIALIZATION OF PLANT-GROWTH PARAMETERS
I
CONSTANT IPER = 0.03
CONSTANT ISHOOT = 0.1, IROOT = 0.05
1. INITIAL SHOOT AND ROOT WEIGHTS, RESPECTIVELY (KG/M**2)
CONSTANT LNGFAC = 13000.0
I LENGTH FACTOR, AS METERS OF ROOT PER KG ROOT WEIGHT
1 (A FACTOR OF 1000 CORRESPONDS TO ABOUT 1 MM ROOT DIAMETER)
CONSTANT RRL = 2.7E-01, 2.3E-01, 2.2E-01, 1.9E-01, 0.06, ...
        .018, 1.0E-02, 1.0E-3, 1.0E-4, 1.0E-3
1 RELATIVE ROOT LENGTH (AS FRACTION OF TOTAL)
CONSTANT RSPFAC = 1.0E-07
' RESPIRATION FACTOR, CONVERTING UNITS AND PROPORTIONING
CONSTANT CONVRT = 0.30
' CONVERSION EFFICIENCY (MASS OF TISSUE PRODUCED PER GRAM INPUT) '
CONSTANT FRG = 0.6666
I FRACTION OF CARBOHYDRATES GOING TOWARD SUPPORT OF SHOOT GROWTH I
CONSTANT AGFAC = 3.0E-07
CONSTANT LEAFTH = 40.0
    ' LEAF THICKNESS--SQ. METERS LEAF AREA/SQ. METER SOIL, FOR EACH
' KG. SHOOT MASS ON THE SAME LAND AREA
CONSTANT GROFAC = 1.0E-05
CONSTANT DTHFAC = 1.0E-10
' FACTOR TO SCALE ROOT DEATH RATE
TABLE FRACTB,1,5/-500.,-200.,-050.,-10.,100.,...
    0.05,0.25,0.70,0.95,0.95/
' UNITS = =, AS A FUNCTION OF CANOPY WATER POTENTIAL
TABLE DTHBGN,1,5/0.0,2.0,5.0,7.0,10.0,\ldots
    0.0,0.03,0.33,0.97,1.00/
l
1 ** INITIALIZATION OF WATER-BALANCE PARAMETERS
1 O
CONSTANT ITHETA = 0.0938, 0.1192, 0.1249, 0.1353, 0.1444, ...
    0.1508,0.1613, 0.1817, 0.2326, 0.3500
' INITIAL SOIL WATER CONTENT (VOLUME FRACTION)
        (INITIALIZED TO VALUES FOUND AFTER 12 DAYS OF DRAINING FROM '
        SATURATION AT 20= WATER IN ALL LAYERS)
CONSTANT DTRDEM = 0.01
1 DAILY TRANSPIRATION DEMAND, M/DAY
CONSTANT DLAY = 21600.
CONSTANT SATCON = 5.3348
1 SATURATED CONDUCTIVITY, AS CM/DAY
CONSTANT ZLAM = 0.64762
' Z(LAMBDA), AFTER LALIBERTE, BROOKS & COREY
CONSTANT TCOM = . 10, 2 *. 15 , 7 *. .20
```

```
' THICKNESS OF EACH VERTICAL LAYER (COMPARTMENT), METERS
CONSTANT \(\mathrm{PB}=21.8258\)
' BUBBLING PRESSURE ( AIR ENTRY VALUE FOR TOP SOIL)
CONSTANT BRMIN \(=-0.30\)
CONSTANT EXTMIN \(=-1.00\)
' THRESHOLD POTENTIAL, THE DRIEST SOIL IN WHICH ROOT GROWTH CAN OCCUR '
CONSTANT \(\mathrm{BR}=1.0 \mathrm{E}-10\)
CONSTANT EXTNRT \(=3.0 \mathrm{E}-04\)
' EXTENSION RATE, FOR NEW ROOT GROWTH FROM ONE LAYER INTO THE NEXT, '
' IN UNITS OF METER/SECOND
CONSTANT \(\mathrm{AA}=7.945089 \mathrm{E}-05, \quad \mathrm{BB}=2.429255\)
' COEFFICIENTS FOR SIGMOID ROOT GENERATION CURVES '
CONSTANT \(\mathrm{B}=1.0 \mathrm{E}-02\)
' CONSTANT, RELATING ROOT CONDUCTIVITY TO ROOT LENGTH, AFTER (GARDNER) '
CONSTANT URRS \(=1.00 \mathrm{E} 11\)
' UNITS FOR RADIAL RESISTANCE
CONSTANT UARS \(=1.00 \mathrm{E} 09\)
' UNITS FOR AXIAL RESISTANCE
CONSTANT MAXPOT \(=-2.0\)
' MAXIMUM ALLOWABLE CANOPY POTENTIAL, ( -2 METER, OR -0.2 BAR) '
TABLE SUCTB, \(1,12 / 0.025,0.05,0.075,0.10,0.15,0.20,0.25,0.30,0.35, \ldots\)
                0.40,0.45,0.50,...
                        20.,5., 3., 1.7,0.6,0.25,0.15,0.10,0.05,0.01,0.0,-1.00/
'TABLE WATRST,1,5/-500.,-200., -100.,0.,100.
            '0.05,0.05,0.95,1.0,1.0/'
- TRANSPIRATION TABLE FOR SENSITIVE CROPS SUCH AS MAIZE OR SOYBEANS \(\mid\)
TABLE WATRST,1,7/-500.,-400., -300., -150., -50.,0.,200.,...
    \(0 ., 0.02,0.06,0.75,0.96,1.00,1.00 /\)
' TRANSPIRATION FOR DROUGHT-TOLERANT CROPS-EG. COTTON OR SORGHUM '
TABLE AVPET,1,2/0.0,366.,0.01,0.01/
' MEASURED PAN EVAPORATION LOSSES - HERE ALL THE SAME TO CHECK MODEL'
TABLE LAIFAC,1,4/0.,3.0,6.0,10.,...
                        0.,0.5,0.9,0.95/
    LEAF AREA INDEX FACTOR, PARTITIONS WATER LOSSS BETWEEN PLANT \& SOIL '
\(1 * * * * * * * * * * \operatorname{INITIAL} \operatorname{SEGMENT} * * * * * * * * * * * * * * * * * '\)
INITIAL
RUNS \(=0\)
FLPFLP \(=-1.0\)
    JDAY = BGNDAY
ICHO \(=(\) ISHOOT + IROOT \() *\) IPER \(/(1 .-\operatorname{IPER})\)
' INITIAL CARBOHYDRATES (KG/M**2), AS DECIMAL FRACTION OF TOTAL MASS.'
        IRTL \(=\) IROOT * LNGFAC
    ' METER OF ROOT/SQUARE METER GROUND AREA AT INITIALIZATION '
        LAI \(=\) ISHOOT \(*\) LEAFTH
    ' LEAF AREA INDEX -- AREA OF LEAF SURFACE/UNIT LAND AREA '
        \(\mathrm{ETA}=2.0+3.0 *\) ZLAM
1
CONSTANT \(\mathrm{NJ}=10\)
' THE NUMBER OF LAYERS(J) IN THE SOIL PROFILE
    \(\operatorname{DEPTH}(1)=.5 *(\operatorname{TCOM}(1))\)
    \(\operatorname{DIST}(1)=\operatorname{DEPTH}(1)\)
    DO \(20 \mathrm{I}=2, \mathrm{NJ}\)
```

```
                DIST(I) =.5*(TCOM(I-1)+TCOM(I))
                DEPTH(I) = DEPTH(I-1) + DIST(I)
    20..CONTINUE
853..FORMAT(/,' INITIALIZE',/,9X,'I',3X,'IPRTL',5X,'RSRT',8X,'IVOLW')
        LINES(2)
        WRITE(6,853)
        DO 30 I = 1,NJ
        IRTEX(I) = 0.0
        IPRTL(I) = IRTL * RRL(I)
' PARTIAL ROOT LENGTH, AT INITIALIZATION
        IVOLW(I) = ITHETA(I)*TCOM(I)
' INITIAL VOLUME OF WATER IN EACH SOIL LAYER
        RRS(I) = URRS / IPRTL(I)
' RADIAL RESISTANCE TO WATER FLOW IN THE ROOT
        ARS(I) = UARS * DEPTH(I) / IPRTL(I)
' AXIAL RESISTANCE -- ALONG THE XYLEM TRANSPORT SYSTEM
        RSRT(I) = RRS(I) + ARS(I)
' RESISTANCE OF THE ROOTS
        LINES(1)
        WRITE(6,454) I,IPRTL(I),RSRT(I),IVOLW(I),TCOM(I),ITHETA(I), ...
            IRTL, RRL(I), DEPTH(I)
    454..FORMAT(3G10.3, 3F10.5,G10.3, 2F10.5, 3G10.3)
        30..CONTINUE
            POTCR = -20.000
            POTCRD= -20.00
' POTENTIAL OF THE CROWN (SHOOT), INITIALIZED BELOW DRIEST SOIL LAYER
| (-20 METERS = -2 BARS)
            DO 10 I = 2,101
        10..LINE(I) = IB
        INITIALIZES PRINT-LINE FOR VERTICAL PLOTS TO BLANK CHARACTER-STRING
            NJJ = NJ+1
' ONE MORE THAN THE NUMBER OF LAYERS IN THE SOIL PROFILE (NJ)
            DO 15 I = 1,NJJ
        15..FLW(I) = 0.0
1 FLOW OF WATER PAST BOTTOM OF EACH LAYER,.INITIALIZED TO 0.0
|
I
END$ ' INITIAL
' * * *
'
I
1 *** DEFINITION OF TIME-BASES *** 
1
l
        HOURC = TIME/3600.0
1 CUMULATIVE HOURS OF SIMULATION TIME
    CLOCK = AMOD(HOURC,24.0)
' CLOCK TIME, IN HOURS
    DAY = HOURC / 24.00
    JDAY = DAY + BGNDAY
```

```
JULIAN DATE, AS DECIMAL FRACTION, DURING THE SIMULATION
    RUN = RUNS
CREATES A REAL-NUMBER COUNTING VARIABLE FOR PRINTER OUTPUT
DERIVATIVE
    TMPFCS \(=10.0 * *((\) TEMP-REFT \() * 0.030103)\)
    TMPFCR \(=10.0 * *((S T E M P-R E F T) * 0.030103)\)
BIOLOGICAL Q-10 -- DOUBLING REACTION RATE AT EACH 10 DEGREE TEMP CHNG'
        TEMP \(=\) REFT \(+((\operatorname{SIN}(2 * \operatorname{PI} *(D A Y-0.375))) *\) RANGE \()\)
    TEMPERATURE FACTOR, MULTIPLIER FOR TEMPERATURE EFFECT
        ** RESERVE LEVELS AND TISSUE GROWTH
        RESL \(=\) SOLCHO / (SOLCHO + ROOTW + SHOOTW)
RESERVE LEVEL, = FREE CARBOHYDRATE IN TISSUES
    SOLCHO \(=\) INTEG ((PHOTSN * PHTCAR - GROWTH - RESP),ICHO)
    PHTCAR \(=30 . / 44\).
SOLUBLE CARBOHYDRATES (FREELY MOBILE, AS METABOLIC RESERVES)
    (KG/SQUARE METER)
    GROWTH \(=\) TOPGRO + TOTRG
TOTAL GROWTH OF BOTH SHOOT AND ROOT SYSTEM
                    ** PHOTOSYNTHETIC ACTIVITY **
    PHOTSN \(=\) RADN * MAXFOT * LAIFAC(LAI) * WATRST(POTCR) / MAXRAD
PHOTOSYNTHETIC RATE (NET CARBON FIXATION, KG/SQUARE METER/SECOND
    \(\operatorname{RADN}=\operatorname{AMAXI}(0.0, \operatorname{SIN}(2 * P I *(D A Y-0.250))) *\) MAXRAD
        ** ROOT AND SHOOT RESPIRATION **
        RESP \(=\) RESPSH + RESPRT
TOTAL RESPIRATION, INCLUDING BOTH SHOOT AND ROOT SYSTEM '
    RESPSH \(=\) SHMRES + SHGRES
RATE OF SHOOT RESPIRATION (KG/SQ METER/SEC)
        (SUM OF GROWTH RESPIRATION AND MAINTENANCE RESPIRATION)
        SHMRES \(=\) SHOOTW * TMPFCS * RSPFAC
        CSTMRS \(=\) INTEG ( SHMRES,0.0)
SHOOT MAINTENANCE RESPIRATION
    SHGRES \(=\) TOPGRO \(*\) CONVRT
' SHOOT GROWTH RESPIRATION
        RESPRT = RTMRES + RTGRES
RESPIRATION OF ROOT SYSTEM
    RTMRES \(=\) ROOTW * RSPFAC * TMPFCR
    CRTMRS \(=\) INTEG(RTMRES,0.0)
ROOT MAINTENANCE RESPIRATION
    RTGRES = TOTRG*CONVRT
ROOT GROWTH RESPIRATION, INCLUDING CHEMICAL CONVERSION AND TRANSPORT'
        ** GROWTH AND DEATH OF SHOOT TISSUE \(* *\)
```

```
    SHOOTW = INTEG( (TOPGRO - SHOOTD),ISHOOT)
WEIGHT OF LIVING SHOOT TISSUE (KG/SQ METER)
    POTCRD = INTEG((POTCR-POTCRD)/DLAY,10.)
    DELAYED CANOPY WATER POTENTIAL
    POTCRE = AMIN1(POTCR,POTCRD)
    EFFECTIVE CANOPY WATER POTENTIAL
    FRAC = FRACTB(POTCRE)
    TOPGRO = TMPFCS * GROFAC * SOLCHO * FRAC
    TOPGRO = TMPFCS * GROFAC * SOLCHO * FRG
    RATE AS (KG/SQ METER/SEC) OF SHOOT (STEMS, LEAVES, AND FRUIT) '
    SHOOTD = SHOOTW * TMPFCS * DTHBGN(LAI) * AGING
SHOOT DEATH RATE (PRINCIPALLY LEAF-DROP DUE TO AGE AND WATER STRESS)'
    AGING = AGFAC * (DAY/30.)
    LAI = SHOOTW * LEAFTH
LEAF AREA INDEX, DIMENSIONLESS (AREA OF LEAF SURFACE/UNIT LAND AREA)'
** GROWTH AND DEATH OF AGGREGATED ROOT SYSTEM *'
    ROOTW = INTEG((TOTRG-ROOTDY),IROOT)
WEIGHT OF LIVE ROOT TISSUE(ALL SOIL LAYERS)
    TOTRG = (1.0 - FRAC) * SOLCHO * GROFAC * TMPFCR
    TOTRG = (1.0 - FRG) * SOLCHO * GROFAC * TMPFCR
TOTAL ROOT GROWTH, SUM OF ROOT WEIGHT IN ALL SOIL LAYERS
    ROOTDY = ROOTW / RESL* DTHFAC * TMPFCR
RATE OF DYING FOR TOTAL ROOT SYSTEM -- MODULATED IN SUMMATION OF '
    DEATH RATES FOR ROOTS IN EACH SOIL LAYER IN A LATER SECTION.
INVERSELY PROPORTIONAL TO CARBOHYDRATE RESERVES--DYING OFF WHEN HUNGRY'
(RATE EXPRESSED AS KG ROOTS/SQUARE METER/SECOND -- WHOLE PLANT) '
** TRANSPIRATION AND WATER LOSS FROM SOIL SURFACE *** '
    TRANSP = WATRST(POTCR) * PET * LAIFAC(LAI)
TRANSPIRATION LOSSES, AS METERS/SECOND
    PET = AMAX1(0.01 * DTRDEM / 86400., PI * RADN * MPANEV / MAXRAD)
POTENTIAL EVAPOTRANSPIRATION, BASED ON TEMPERATURE (+ RADIATION)
    (NOT LESS THAN 1= OF AVERAGE TRANSP. DEMAND--NEGATIVES ELIMINATED) '
        CUMPET = INTEG(PET,0.0)
CUMULATIVE POTENTIAL EVAPOTRANSPIRATION -- COMPARE OUTPUT WITH AVPET'
        MPANEV = AVPET(JDAY) / 86400.
MEASURED POTENTIAL EVAPOTRANSPIRATION IN FIELD (METERS PER DAY) '
    SLEVAP = PET * (1.0 - LAIFAC(LAI))
SOIL EVAPORATION (METERS/SEC), PET REDUCED BY LEAF SHADING '
SOIL EVAPORATION (MLTERS/SEC), PET REDUCED BY LEAF SHADING ,
            ** SOIL WATER MOVEMENT CALCULATIONS ** 1
            SOIL WATER MOVEMENT CALCULATIONS *** ,
    VOLW = INTVC ( NFLW ,IVOLW)
VOLUME OF WATER STORED IN EACH SOIL LAYER
```

```
l
\prime ** OOMPUTE SOIL WATER CONTENT, POTENTIALS, AND CONDUCTIVITY
PROCEDURAL(THETA, POTM, POTH, MPOT, RK, COND ...
        = TIME, PB)
        DO 100 I = 1,NJ
        THETA(I) = VOLW(I)/TCOM(I)
        POTM(I)=-SUCTB(THETA(I ))
        POTH(I) =POTM(I) - DEPTH(I)
    100..CONTINUE
!
1 ** COMPUTE SOIL HYDRAULIC CONDUCTIVITY **
        DO 85 I = 1, NJ
        MPOT = -POTM(I) * 100.0
        IF (MPOT.LE. 0.0) GO TO 84
        RK(I) = (PB/MPOT) ** ETA
' RELATIVE CONDUCTIVITY (AS A FRACTION OF SATURATED CONDUCTIVITY) '
        GO TO 87
    84..RK(I) = 1.0
        RELATIVE CONDUCTIVITY CAN NEVER BE MORE THAN 1.0; '
THUS, SATURATED CONDUCTIVITY APPLIES IF MATRIC POTENTIAL IS POSITIVE '
    87..CONTINUE
        RK(I) = AMIN1(1.00, RK(I))
' CONDUCTIVITY IS LIMITED TO A MAXIMUM OF THE SATURATED CONDUCTIVITY '
    COND(I) = RK(I) * SATCON / 8.6400E06
' SOIL HYDRAULIC CONDUCTIVITY, METERS/SECOND
    85..CONTINUE
END $ 'PROCEDURAL'
\prime}** COMPUTE VERTICAL SOIL WATER FLOW (DARCIAN) *** ',
PROCEDURAL(AVCOND, FLW, NFLW= POTH)
            DO 110 I = 2,NJ
            AVCOND(I) =.5*(COND(I-1) + COND(I))
            FLW(I) = AVCOND(I) * (POTH(I-1)-POTH(I)) / DIST(I)
110..CONTINUE
            IF (POTM(1) .GT. -10.0) FLW(1)=-SLEVAP
            IF (POTM(1) .LE. -10.) FLW(1)=FLW(2)
' WATER FLOW OUT THE TOP IS LIMITED BY SUPPLY IF TOP LAYER IS DRY
            FLW(NJJ) = 0.000000
            DO 120 I = 1,NJ
                NFLW(I) = FLW(I) - FLW(I+1) - RTEX(I)
    120..CONTINUE
END $ 'PROCEDURAL'
    ** PARTITIONING AGGREGATE ROOT GROWTH BETWEEN SOIL LAYERS **
    PRTL = INTVC(NETGRO,IPRTL)
', PARTIAL ROOT LENGTH, IN EACH SOIL LAYER -- SUM OF GROWTH LESS DEATH
PROCEDURAL(BIRTH,EXTENS,RTGRO,SUMRG,RTDTH,SUMRD,NETGRO, . ..
    W,SUMRTG,SUMRTD = POTM)
```

```
, *** ROOT GROWTH IN EACH LAYER **
    W = AMAX1(0.0, (POTM(2) - EXTMIN))
    DO 1010 I=1,NJ
    X = AMAX1(0.0, (POTM(I) - BRMIN))
    XX = AMAX1(0.0, (POTM(I) - EXTMIN))
    BIRTH(I) = BR * ( 1.0 - EXP ( -AA*X**BB ) )
1010..EXTENS(I) = EXTNRT * ( 1.0 - EXP ( -AA*XX**BB ) )
        RTGRO(1) = PRTL(1) * BIRTH(1)
        SUMRG = RTGRO(1)
' SUMMATION OF INSTANEOUS ROOT GROWTH RATES, OVER ALL SOIL LAYERS
' (EXPRESSED AS METERS ROOTS/SQUARE METER SURFACE/SECOND)
    DO 647 I = 2,NJ
    RTGRO(I) = (PRTL(I-1)*EXTENS(I) + PRTL(I)*BIRTH(I))
' GROWTH EXPRESSED AS METERS/SEC IN EACH SQUARE METER OF EACH LAYER
647..SUMRG = RTGRO(I) + SUMRG
' TOTAL INCREASE, WHOLE PLANT, IN METERS/SQ. METER/SECOND
            SUMRTG = 0.0
            DO 648 I = 1,NJ
            IF (SUMRG.EQ.0.00) GO TO 648
            RTGRO(I) = RTGRO(I) * TOTRG/SUMRG * LNGFAC
' (BRINGS ACTUAL ROOT GROWTH IN EACH LAYER INTO LINE WITH TOTAL
' PHOTOSYNTHATE AVAILABLE AT ANY GIVEN TIME).
            SUMRTG = SUMRTG + RTGRO(I)
    648..CONTINUE
I
! ** ROOT DEATH IN EACH LAYER ** *
    SUMRD = 0.0
        DO 649 I = 1, NJ
        RTDTH(I) =PRTL(I) * DTHFAC * TMPFCR
' ROOT DEATH, AS METERS/SECOND LOST FROM EACH LAYER
    649..SUMRD = SUMRD + RTDTH(I)
        SUMRTD = 0.0
        DO 651 I = 1, NJ
        IF (SUMRD.EQ.O.) GO TO 651
        RTDTH(I) = RTDTH(I) * ROOTDY/SUMRD * LNGFAC
' SCALES ACTUAL DEATH RATE TO TOTAL AGGREGATE REQUIRED FOR C-BALANCE
            SUMRTD = SUMRTD + RTDTH(I)
' TOTAL FOR PLANT, AS METERS/SQ. METER/SECOND
651..CONTINUE
, %% SUMMARY OF GROWTH AND DEATH IN EACH LAYER %
        DO 653 I = 1,NJ
653..NETGRO(I) = RTGRO(I) - RTDTH(I)
        NET CHANGE IN ROOT LENGTH, AS METERS/SECOND CHANGE IN EACH LAYER.
END $ 'PROCEDURAL'
I
1 ** ROOT SYSTEM RESISTANCE AND WATER UPTAKE **
PROCEDURAL(RSSL, PTOTL, RSRT = COND,SUMRG)
```

```
        DO 102 I = 1,NJ
        RSSL(I) = 1./(B*COND(I)*PRTL(I))
        PTOTL(I) = POTH(I)
        NOTE THAT PTOTL IS THE SAME AS HYDRAULIC POTENTIAL IN THIS VERSION
        RRS(I) = URRS / PRTE(I)
    ' RADIAL RESISTANCE TO WATER FLOW IN THE ROOT
        ARS(I) = UARS * DEPTH(I) / PRTL(I)
    ' AXIAL RESISTANCE -- ALONG THE XYLEM TRANSPORT SYSTEM
    RSRT(I) = RRS(I) + ARS(I)
' COMBINED AXIAL AND CONDUCTIVE RESISTANCE OF ROOTS IN THIS LAYER
    102..CONTINUE
END $ 'PROCEDURAL'
!
I
' ** CALCULATION OF POTCR AND PARTITIONING OF ROOT WATER UPTAKE
    CUMREM = INTEG(SUMR,0.0)
' CUMULATIVE WATER REMOVAL (BY ROOT SYSTEM) FROM ALL SOIL LAYERS
PROCEDURAL( SUMR,DIFF,DIF,RTEX,POTRT =...
            POTH, TRANSP, RUN, RSRT)
        COUNT = 0.0
        FLPFLP = -FLPFLP
    115..CONTINUE
            COUNT = COUNT + 1.0
            IF ( COUNT .LT. 100.0 ) GO TO 116
            GO TO 165
' IN CASE THE LOOP DOES NOT CONVERGE IN 100 TRIES, GO AHEAD ANYWAY
116..CONTINUE
            SUMR = 0.0
            DO 150 J = 1,NJ
            I = J
            IF ( FLPFLP .EQ. 1.0 ) I = NJ - J + 1
            RTEX(I) = AMAXI(0.0 ,(POTH(I) - POTCR) / (RSSL(I) + RSRT(I) ) )
1 ROOT EXTRACTION, M/SECOND
            SUMR = SUMR + RTEX(I)
' SUM OF WATER REMOVALS BY ROOTS IN ALL LAYERS
            DIFF = TRANSP - SUMR
            IF (SUMR .LT. TRANSP) RTEX(I) = AMIN1(RTEX(I),DIFF)
150..CONTINUE
I
' FOR EACH LAYER, WATER EXTRACTION IS ASSUMED ON THE BASIS OF CURRENT
' VALUE FOR CANOPY POTENTIAL. ITERATION WILL CONTINUE UNTIL EQUAL.
            DIF = (SUMR - TRANSP) / TRANSP
            IF (COUNT.GT.5.0) GO TO 165
            IF ( ABS(DIF) .LE. ERROR ) GO TO 165
            IF ( DIF ) 160 , 165 , 160
' ADJUSTMENT OF CANOPY WATER POTENTIAL UP OR DOWN AS NEEDED TO BALANCE'
160..POTCR = AMIN1((POTCR - DIF*POTCR*CE),MAXPOT)
    GO TO 115
165..CONTINUE
    DO 170 I = 1,NJ
    POTRT(I) = POTCR + RTEX(I) * RSRT(I)
170..CONTINUE
```

```
END $ 'PROCEDURAL'
* *** SUMMARY OF WATER MOVEMENT AND EVAPORATIVE LOSSES
    CRTEX = INTVC ( RTEX ,IRTEX)
    CUMULATIVE ROOT EXTRACTION
    EVAP = AMIN1(-FLW(1), SLEVAP)
    EVAPORATION FROM SOIL SURFACE - LIMITED BY AVAILABILITY OF WATER '
' (COMING FROM DEEPER SOIL LAYERS) OR BY THERMAL INSOLATION AT SURFACE '
    CEVAP = INTEG( EVAP,0.0)
' CUMULATIVE EVAPORATION FROM SOIL SURFACE
    FLW8P = AMAX1 (0.0,FLW(8))
    DRAIN = INTEG (FLW8P,0.0)
' INTERNAL DRAINAGE, AS WATER PASSES THE BOTTOM OF THE 7TH LAYER ।
    FLW8N = - AMIN1(0.0,FLW(8))
    CAPRIS = INTEG (FLW8N,0.0)
' CAPILLARY RISE, PAST THE 8TH LAYER
    CUMTRN = INTEG (TRANSP,0.0)
    DRAING = FLW8P
' CUMULATIVE TRANSPIRATION, AS M/SQUARE METER
' XYZ=DEBUG(02,0.0)'
' ZYX=DEBUG(01,3600.)'
END$'DERIVATIVE'
TERMT(HOURC.GT.120.0.OR.POTCR.LT.-300..OR.SOLCHO.LT.1.0E-07.OR....
        SHOOTW.LT.0.0001.OR.TOPGRO.LT.-1.0E-10.OR.TOTRG.LT.-1.0E-18)
' THE SIMULATION WILL TERMINATE WHEN THE PLANT WATER POTENTIAL DROPS'
' BELOW -300 METER WATER POTENTIAL(OR -30 BAR),OR WHENEVER ALL
' SOLUBLE CARBOHYDRATE IS EXPENDED ( NO FOOD IN STORAGE)
I
* ** VERTICAL GRADIENT PLOTTING INSTRUCTIONS **
I
PROCEDURAL(YY,Y=OUTF ,THETA, POTM, CRTEX, PTOTL,FLW, PRTL,TCOM)
    YY = PULSE ( 0.0 , OUTF , 600. )
    IF ( YY .EQ. 0.0 ) GO TO 1200
    IF (TIME.LT.OUTF) GO TO }120
    IF (KEEP.NE.1) GO TO }120
    OUTF = OUTF + OUTF
    RUNS = 1
    COUNT = 1
' FOR VARIABLE-FREQUENCY OUTPUT PLOTS
    DO 1000 IFUN = 1,6
' THE ORDER WILL BE THETA PPOTM CRTEX PTOTL FLW PRTL
    GO TO ( 500,550,650,700,750,850 ) , IFUN
    500..DO 505 I=1,NJ
    505.. Y(I) = THETA(I)
    WRITE(6,1505)
1505..FORMAT('1', /, 56X, 'THETA VS. DEPTH', /)
    GO TO 900
    550..DO 555 I=1,NJ
    555..Y(I) = - POTM(I)
    WRITE (6, 1555)
1555..FORMAT('1',/,56X,'-POTM (METERS) VS. DEPTH', /)
```

GO TO 900
650..DO $655 \mathrm{I}=1, \mathrm{NJ}$
655..Y(I) = CRTEX(I)

WRITE (6,1655)
1655..FORMAT('1',/,56X,'CUMULATIVE ROOT EXTRACTION, METERS VS. DEPTH',/) GO TO 900
700..DO $705 \mathrm{I}=1$, NJ
705..Y(I) =-PTOTL(I)

WRITE (6,1705)
1705..FORMAT('1',/,56X,'TOTAL WATER POTENTIAL AS A FUNCTION OF DEPTH',/) GO TO 900
750..DO $755 \mathrm{I}=1, \mathrm{NJ}$
755..Y(I) $=F L W(I)$

WRITE $(6,1755)$
1755..FORMAT('1',/, 56X, 'VERTICAL WATER FLUX RATE, POSITIVE DOWN',/) GO TO 900
850..DO $855 \mathrm{I}=1$, NJ
855..Y(I) $=\operatorname{PRTL}(I) / T C O M(I)$ WRITE $(6,1855)$
1855..FORMAT('1',/, 41X, 'PARTIAL ROOT LENGTH, METERS/SQ. METER ', ... 'IN EACH LAYER', /)
900..CONTINUE WRITE $(6,905)$ HOURC, RUN, IFUN
 I2, //)
SCAAL (IFUN) $=($ SMAX (IFUN) $-\operatorname{SMIN}(I F U N)) / 75.0$ DO $950 \mathrm{I}=1, \mathrm{NJ}$ $\mathrm{IL}=(\mathrm{Y}(\mathrm{I})-\operatorname{SMIN}(I F U N)) / \operatorname{SCAAL}(I F U N)+2.0$ IF (IL.LE.2) $\mathrm{IL}=2$ IF (IL.GE. 101 ) IL = 101 $\mathrm{J}=0.5+\mathrm{TCOM}(\mathrm{I}) * 100.0 / 4.0$ LINE(IL) = IX
922..J = J-1

IF (J) 931,931,925
925...WRITE (6, 926)
926..FORMAT(' $1^{\prime}$ ) GO TO 922
931..WRITE (6,935) $\operatorname{DEPTH}(I),(\operatorname{LINE}(K), K=1,101), Y(I)$
935..FORMAT(2H , F9.4,3X,101A1,2X,E12.5)
$\operatorname{LINE}(I L)=I B$
950..CONTINUE
1000.. CONTINUE
1200. . CONTINUE RUNS $=$ RUNS +1
END\$ 'PROCEDURAL'
ENDS' DYNAMIC'
$1 * * * * * * * * \operatorname{TERMINAL} \operatorname{SEGMENT} * * * * * * * * * * * * * * * * 1$
'
TERMINAL
END\$' TERMINAL
END\$' OF PROGRAM
//GO.FT99F001 DD SYSOUT=(C,,1111)
//GO.SYSIN DD *

PREPAR TIME,HOURC,RADN,POTCR,SOLCHO,SHOOTW,ROOTW,PHOTSN,POTCRE, . . . TOPGRO, TOTRG, SHOOTD, ROOTDY, NETGRO, CUMREM, CUMTRN, CEVAP, DRAIN, . . . RESP, FRAC, THETA, SHMRES, SHGRES, RTMRES, RTGRES
SET TITLE= ' WATER UPTAKE AND ROOT GROWTH IN A HOMOGENEOUS SOIL PROFILE' OUTPUT TIME,HOURC,RADN, PHOTSN, POTCR, SOLCHO, SHOOTW,
ROOTW, 'NCIOUT' $=10$
START
SET CALPLT=.TRUE., PENCPL=.TRUE., XINCPL=10.0,YINCPL=7.5,NPCCPL=50,...
TTLCPL=.TRUE., SYMCPL=.TRUE.
SET TITLE $=$ ' NET-PHOTOSYNTHESIS AND RESPIRATION (KG/M2/SEC)
PLOT 'XAXIS' = HOURC,'XHI' = 120., PHOTSN,RESP,'SAME', SOLCHO
SET TITLE $=$ 'SHOOT MAINTENANCE AND GROWTH RESPIRATION
PLOT 'XAXIS' = HOURC,'XHI'=120., SHGRES,RTGRES,RTMRES,SHMRES,'SAME'
SET TITLE $=$ 'FACTORS INFLUENCING BIOMASS PARTITIONING
PLOT 'XAXIS' = HOURC,'XHI'=120., POTCR, POTCRE,'SAME', FRAC
SET TITLE $=$ ' TISSUE GROWTH AND BIOMASS PARTITIONING
PLOT 'XAXIS' = HOURC,'XHI'=120.,TOPGRO,TOTRG,SHOOTD,ROOTDY,'SAME'
SET TITLE $=$ ' NET INCREASE IN ROOT LENGTH (METER/METER2)
PLOT 'XAXIS' = HOURC,'XHI'=120., NETGRO(10), NETGRO(9), NETGRO(8),...
NETGRO(7), NETGRO(6), NETGRO(5), NETGRO(4),NETGRO(3),NETGRO(2),...
NETGRO(1),'SAME'
SET TITLE = 'SOIL WATER CONTENT
PLOT 'XAXIS' = HOURC,'XHI'=120.,THETA(04),THETA(3),THETA(2),...
THETA(1), THETA(10), THETA(9), THETA(08), THETA(7), THETA(6), ...
THETA(5),'SAME'

SET TITLE = ' SIMULATED CUMULATIVE WATER BALANCE : TRANSPIRATION...
AND UPTAKE'
PLOT 'XAXIS' = HOURC,'XHI'=120., CUMREM, CUMTRN, CEVAP, DRAIN,'SAME' STOP

GLOSSARY OF TERMS USED IN SIMULATION MODEL

| VARIABLE | DESCRIPTION | UNIT |
| :---: | :---: | :---: |
| AA | Coefficient for sigmoid root generation curve | (dimension1ess) |
| AAA | Procedure statement | - |
| ABS | FORTRAN function - absolute value | - |
| ABSERR | Absolute error (CSMP variable for integration control) | - |
| AFGEN | CSMP function generator (CSMP library linear interpolation) | - |
| AGE | Cumulative days of simulation time | day |
| AGFAC | Aging factor, parameter controlling leaf aging | $\mathrm{kg} /(\mathrm{kg} \mathrm{s})$ |
| AGING | Relative aging factor, modifying shoot death rate | day/day |
| ALPHA | Constant in relative conductivity equation | 1/m |
| ALOG | FORTRAN function - natural logarithm | - |
| AMAX1 | ```FORTRAN function - maximum real number variable``` | - |
| AMIN 1 | FORTRAN function - minimum real number variable | - |
| AMOD | FORTRAN function - remaindering function | - |
| AND | CSMP function - logic AND function | - |
| ARS | Axial resistance to water flow through roots (xylem flow resistance) | sec |
| ATAN | FORTRAN function - ARCTANGENT | - |
| AVCOND | Average conductivity for water flow between soil compartments | $\mathrm{m} / \mathrm{sec}$ |
| AVPET | Average potential evapotranspiration, as measured daily | m/day |
| B | Constant, relating soil-root conductivity to length of root | 1/m |
| BB | Coefficient for sigmoid generation curve | - |
| BGNDAY | Julian date at the beginning of the simulation run | day |
| BIRTH | Branching rate (Formation of new roots in same soil layer) | $\mathrm{m} / \mathrm{sec}$ |
| BR | Branching rate parameter | $\mathrm{m} / \mathrm{sec}$ |
| BRMIN | Lowest soil water potential at which root branching occurs (new root tissue) | $m(k \underset{3}{ } \mathrm{a} * 10)$ |
| BULKDS | Bulk density of the soil | $\mathrm{kg} / \mathrm{m}^{3}$ |
| BULKF | Table for bulk density as a function of depth | - |


| CAPRIS | Cumulative capillary rise (past the bottom layer) | m |
| :---: | :---: | :---: |
| CEVAP | Cumulative evaporation from soil surface | m |
| CF | Correction factor - iteration loop | - |
| CLOCK | Clock time |  |
| CMRAIN | Measured daily rainfall | m/day |
| COND | Soil hydraulic conductivity | $\mathrm{m} / \mathrm{sec}$ |
| CONVRT | Relative growth efficiency <br> (kg biomass/kg carbohydrate respired) | $\mathrm{kg} / \mathrm{kg}$ |
| COS | FORTRAN function - cosine | - |
| COUNT | Counter for iteration loop | - |
| CRC | Current radiation under a clear sky | Joule/(m2 sec) |
| CRO | Current radiation under an overcast sky | Joule/( $\mathrm{m}^{2} \mathrm{sec}$ ) |
| CRTEX | Cumulative root extraction | m |
| CRTMRS | Cumulative root maintenance respiration | $\mathrm{kg} / \mathrm{m}^{2}$ |
| CSDC | Cosine of declination | - |
| CSLT | Cosine of latitude | - |
| CSTMRS | Cumulative shoot maintenance respiration | $\mathrm{kg} / \mathrm{m}^{2}$ |
| CTRAN | Cumulative transpiration | $\mathrm{m}\left(\mathrm{H}_{2} \mathrm{O}\right)$ |
| CUMPET | Cumulative potential evapotranspiration | $\mathrm{m}\left(\mathrm{H}_{2} \mathrm{O}\right)$ |
| CUMRAD | Cumulative daily total radiation | Joule/m ${ }^{2}$ |
| CUMREM | Cumulative water removal ( by root system ) from all soil layers | $m\left(\mathrm{H}_{2} \mathrm{O}\right)$ |
| C0 | Auxiliary variable for the calculation of photosynthesis under a clear sky | $\mathrm{kg} \mathrm{CO} 2 /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| C1 | Auxiliary variable for the calculation of photosynthesis under a clear sky | $\mathrm{kg} \mathrm{CO} 2 /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| C2 | Auxiliary variable for the calculation of photosynthesis under a clear sky | $\mathrm{kg} \mathrm{CO} 2 /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| DATA | FORTRAN statement - data input |  |
| DAY | Day of the year during simulation | day |
| DAYRAD | Daily total radiation | Joule/(m ${ }^{2}$ day) |
| DAYRAI | Daily total rainfall | m/day |
| DAYS | Table for number of days per month | - |
| DEBUG | CSMP statement - controls error debugging | - |
| DEC | Declination of the sun with respect to the equator | degree |
| DELAY | Delay time for computation of effective canopy water potential | sec |
| DELMAX | Maximum time-step for integration routine | sec |
| DELMIN | Minimum time-step for integration | sec |
| DELT | Timestep for integration | sec |
| DEPTH | Depth to midpoint of soil layer, measured from soil surface | m |
| DEPTHG | Factor accounting for increased resistance to soluble carbohydrates with deeper roots | $\mathrm{m} / \mathrm{m}$ |
| DFCLTB | Table for diffuse visible radiation under a standard clear sky | - |
| DFOVTB | Table for diffuse visible radiation under a standard overcast sky | - |
| DIF | Difference between root extraction rate and transpiration rate | $\mathrm{m} / \mathrm{sec}$ |

DIFCL Diffuse visible radiation under a standard clear sky
DIFF Relative difference between root extraction rate and transpiration rate
DIFON Diffuse near-infrared radiation under a standard overcast sky
DIFOV Diffuse visible radiation under a standard overcast sky
DIMENSION (FORTRAN-statement to define arrays)
DIST Distance of flow between two adjacent soil layers
DKPHOT Dark respiration rate of the leaves
DLLA Leaf area of shaded leaves
DLYTOT MACRO for the computation of daily totals
DRAD
DRADI
DRAIN
DRAING Instantaneous drainage rate (past bottom of lowest soil layer)
DRC Daily total global radiation under a clear sky
DRCI Initial daily total global radiation under a clear sky
DRCP Daily total global radiation under a clear sky of previous day
DRO Daily total global radiation under an overcast sky
DROI Initial daily total global radiation under an overcast sky
DROP Daily total global radiation under an overcast sky of previous day
DRYWT Total dry matter of the plant
DTBL Table of shoot death versus leaf area index
DTHBGN
Relative shoot death rate
DTHFAC Relative root death rate
DTR Daily total global radiation measured (constant over a day)
DTRDEM Daily transpiration demand (average, parameter for minimum)
DTRR Daily total global radiation measured
ECON Base of natural logarithm , 'e'
EFF Efficiency of photosynthesis at light compensation point
ERROR Maximum allowable error in iteration loop (POTCR computation)
ETA Soil porosity
EVAP Evaporation from soil surface
EXP FORTRAN function - exponentiation
EXTENS Extension rate for root growth into the next soil layer
EXTMIN Threshold soil water potential for root extension into next soil layer
EXTNRT Extension rate parameter, for root growth into adjacent layer

$$
\begin{aligned}
& \text { Joule/( } \left.\mathrm{m}^{2} \mathrm{sec}\right) \\
& \text { (dimensionless) } \\
& \text { Joule/( } \left.\mathrm{m}^{2} \mathrm{sec}\right) \\
& \text { Joule/( } \left.\mathrm{m}^{2} \mathrm{sec}\right) \\
& \text { - } \\
& \text { m } \\
& \begin{array}{l}
\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right) \\
\mathrm{m}^{2} / \mathrm{m}^{2}
\end{array} \\
& \text { - } \\
& \text { Joule/m }{ }^{2} \\
& \text { Joule/m }{ }^{2} \\
& \text { m } \\
& \mathrm{m} / \mathrm{sec} \\
& \text { Joule/m }{ }^{2} \\
& \text { Joule/m }{ }^{2} \\
& \text { Joule/m }{ }^{2} \\
& \text { Joule/m }{ }^{2} \\
& \text { joule/m }{ }^{2} \\
& \text { joule/m }{ }^{2} \\
& \mathrm{~kg} / \mathrm{m}^{2} \\
& \mathrm{~kg} /(\mathrm{kg} \mathrm{sec}) \\
& \mathrm{kg} /(\mathrm{kg} \mathrm{sec}) \\
& \text { Joule/(m2 day) } \\
& \text { m/day } \\
& \text { Joule/(m }{ }^{2} \text { day) } \\
& \mathrm{kg} /(\mathrm{J} \mathrm{~s}) \\
& \mathrm{m}^{3} / \mathrm{m}^{3} \\
& \mathrm{~m} / \mathrm{sec} \\
& \text { - } \\
& \mathrm{m} / \mathrm{sec} \\
& \text { m ( } \mathrm{kPa} * 10 \text { ) } \\
& \mathrm{m} / \mathrm{sec}
\end{aligned}
$$

| FCL | Fraction of the time that the sky is clear | - |
| :---: | :---: | :---: |
| FGLOAD | ```CMSP Function - input for function generator table``` | - |
| FINISH | Conditions for termination of simulation run | - |
| FINT | Extension coefficient for light in canopy | (dimensionless) |
| FINTIM | Total duration of simulation run | sec |
| FLPFLP | Flipflop control statement for iteation loop | - |
| FLW | Flow of water past bottom of each soil layer | $\mathrm{m} / \mathrm{sec}$ |
| FLWNJN | ```Capillary rise ( Past the bottom soil layer, negative flow up)``` | m |
| FOV | Fraction of time that the sky is overcast | - |
| FRAC | Fraction of carbohydrates remaining in the shoot ( computed ) | $\mathrm{kg} / \mathrm{kg}$ |
| FRACTB | Table for carbohydrate partitioning based upon canopy water potential | - |
| FRG | Set constant for fraction of carbohydrates remaining in the shoot | - |
| GROFAC | Relative consumption rate of reserves | $\mathrm{kg} /(\mathrm{kg} \mathrm{sec})$ |
| GROWTH | Total growth rate of both root and shoot systems | $\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| HOUR | Clock time | hour |
| HOURS | Cumulative hours of simulation time | hour |
| HSUN | Height of the sun | degree |
| I | Index of soil layer (ordinal number) | - |
| IB | Index for gradient plotting | - 2 |
| I CHO | Initial mass of carbohydrates | $\mathrm{kg} / \mathrm{m}^{2}$ |
| IFUN | Index for gradient plotting | - |
| IDAY | Age of the plant at start of simulation | day |
| IL | Index for gradient plotting | - |
| IMPULS | CSMP function - impuls generator | - |
| INSW | CSMP function - input switch generator | - |
| INTLZ | Procedure statement | - |
| IPER | Initial fraction of soluble carbohydrates | - 2 |
| IPRTL | Initial root length per layer | $\mathrm{m} / \mathrm{m}^{2}$ |
| IRFAC | Minimum soil water potential to trigger irrigation | kPa |
| IRMIN | Minimum soil water potential to trigger irrigation (same as IRFAC, but in m) | m |
| IROOT | Initial root mass | $\mathrm{kg} / \mathrm{m}^{2}$ |
| IRQUAN | Volume of water applied during irrigation pulse | $\mathrm{cm}^{3} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| IRTL | Initial total root length | $\mathrm{m} / \mathrm{m}^{2}$ |
| IRTVL | Initial total root volume | $\mathrm{m}^{3} / \mathrm{m}^{2}$ |
| IRTWT | Initial total root mass | $\mathrm{kg} / \mathrm{m}^{2}$ |
| ISHOOT | Initial shoot mass | $\mathrm{kg} / \mathrm{m}^{2}$ |
| ITHETA | Initial volumetric water content of the soil | $\mathrm{m}^{3} / \mathrm{m}^{3}$ |
| IVOLW | Initial amount of water in each layer | $\mathrm{m}^{3} / \mathrm{m}^{2}$ |
| IX | Index for gradient plotting | - |


| J | Index of soil layer (ordinal number) | - |
| :---: | :---: | :---: |
| JDAY | Day of the year during simulation (integer number) | day |
| JJ | Day of the month during simulation | day |
| JULIAN | Day of the year during simulation | day |
| K | Runner in DO loop | - |
| KEEP | CSMP integration control statement ( $0=$ trial integration, $1=$ advance time step) | - |
| LAI | Leaf area index | $\mathrm{m}^{2} / \mathrm{m}^{2}$ |
| LAIFAC | Leaf area index factor for partitioning of water loss between plant and soil | (dimensionless) |
| LAITBL | Table relating leaf area index and water loss between plant and soil | - |
| LAT | Latitude of experimental plot | degree |
| LEAFTH | Specific leaf area | $\mathrm{m}^{2} / \mathrm{kg}$ |
| LEAFW | Mass of the leaves | $\mathrm{kg} / \mathrm{m}^{2}$ |
| LFCL | Fraction of time that the sky is clear, restrained between 0 and 1 | (dimensionless) |
| LFOV | Fraction of time that the sky is overcast, restrained between 0 and 1 | (dimensionless) |
| LIMIT | CSMP function - defining limitation or saturation of a system | - |
| LINE | Variable for gradient plotting | - |
| LNGFAC | Length/mass ratio of the roots | $\mathrm{m} / \mathrm{kg}$ |
| LSNHS | Sine height of the sun of the previous day | degree |
| MAXPOT | Maximum allowable canopy water potential | $m\left(M P a * 10^{2}\right)$ |
| MAXRAD | Maximum light flux density ( during a day) | $\mathrm{J} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| MAXSTM | Measured maximum soil temperature | degree ( ${ }^{\circ} \mathrm{C}$ ) |
| MAXTEM | Measured maximum air temperature | degree ( ${ }^{\circ} \mathrm{C}$ ) |
| MAXTMP | Measured maximum air temperature table | - |
| MINRTL | Minimum root length for root expansion between two adjacent soil layers | m |
| MINSTM | Measured minimum soil temperature | degree ( ${ }^{\circ} \mathrm{C}$ ) |
| MINTEM | Measured minimum air temperature | degree ( ${ }^{\circ} \mathrm{C}$ ) |
| MINTMP | Measured minimum air temperature table | - |
| MNSTMP | Measured minimum soil temperature table | - |
| MONTH | Integer number presentation of month | - |
| MPANEV | Estimated pan evaporation (a scaling factor for PET) | m/day |
| MPOT | Matric potential of the soil in each layer (computed from soil water content) | $\mathrm{m}(\mathrm{kPa} * 10)$ |
| MTH | Real number presentation of month | - |
| MTIME | Macro for the computation of day and month |  |
| MXPHOT | Maximum photosynthetic rate | $\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| MXSTMP | Measured maximum soil temperature table | - |
| MU | ```Constant 'm' in relative conductivity equation``` | (dimensionless) |

NALARM
NETGRO

NETVLG
NETWTG
NFLW

NJ

NJJ

NNJ

NOT
NU

OUTDEL OUTF

00

01

02

PARTDS
PB

PET
PEV
PEVAP
PEVV
PEVVV

PHOTC

PHOTD

PHOTS

PHOTSH

PHOTSM

PHOTSN
PHTCAR
PI

POROS
POTCR
POTCRD

CSMP flag
Net change in root length per layer ( growth - death )
Net change in root volume per layer
Net change in root mass per layer
Net flow of water into each soil layer ( Darcian movement only )
Number of layers comprising the soil profile
Number of layers in the soil profile plus one
Number of layers in the soil profile minus one
CSMP Function
Constant ' $n$ ' in relative conductivity equation

Time interval for output points on CSMP plots Output function for vertical gradient plotting
Auxiliary variable to calculate photosynthesis under an overcast sky
Auxiliary variable to calculate photosynthesis under an overcast sky
Auxiliary variable to calculate photosynthesis under an overcast sky

Particle density
Bubbling pressure (air entry value for saturated soil)
Potential evapotranspiration
Measured pan evaporation table
Measured pan evaporation
Measured pan evaporation (constant over a day)
Photosynthetic rate under a completely clear sky
Photosynthetic rate under a completely clear sky for diffuse radiation
Photosynthetic rate under a completely clear sky for direct radiation
Photosynthetic rate under a completely overcast sky
Maximum daily photosynthetic rate (net fixation)
Photosynthetic rate (net carbon fixation)
Photosynthetic carbon conversion factor (molecular weight ratio)
Circumference of a circle, divided by its diameter
Porosity of the soil
Canopy plant water potential
Delayed canopy water potential
$\mathrm{m} / \mathrm{sec}$
$\mathrm{m}^{3} / \mathrm{sec}$
$\mathrm{kg} / \mathrm{sec}$
$\mathrm{m} / \mathrm{sec}$
-
-
-
-
(dimensionless)
sec
sec
$\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$
$\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$
$\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$
$\mathrm{kg} / \mathrm{m}^{3}$
$\mathrm{cm}\left(\mathrm{kPa} * 10^{-1}\right)$
$\mathrm{m} / \mathrm{sec}$
-
m/day
m/day
m/day
$\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$
$\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$
$\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$
$\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$
$\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$
$\mathrm{kg} \mathrm{CO} 2 /\left(\mathrm{m}^{2} \mathrm{sec}\right)$
(dimensionless)
$\mathrm{m}^{3} / \mathrm{m}^{3}$
$\mathrm{m}\left(\mathrm{MPa} * 10^{-2}\right)$
m

| POTCRE | Effective canopy water potential | m |
| :---: | :---: | :---: |
| POTH | Hydraulic potential head in each soil layer | m |
| POTM | Matric potential of the soil in each layer | m |
| POTMAR | Minimum matric potential of top soil layer | m |
| POTRT | Water potential of the roots | m |
| POVC | Auxiliary variable to calculate photosynthesis | - |
| PRDEL | Time interval for outputting print results | sec |
| PROC1 | Procedure statement | - |
| PROC2 | Proçedure statement | - |
| PROC3 | Procedure statement | - |
| PROC4 | Procedure statement | - |
| PROC5 | Procedure statement |  |
| PRTL | Root length per layer | $\mathrm{m} / \mathrm{m}^{2}$ |
| PS | Auxiliary variable for the calculation of photosynthesis | (dimensionless) |
| PSH | Auxiliary variable for the calculation of photosynthesis | (dimensionless) |
| PTOTL | Total soil water potential (grav. + osm. + matric) for each soil layer | $\mathrm{m}(\mathrm{kPa} * 10)$ |
| PULSIR | Pulse to trigger irrigation after a defined time interval | - |
| PULSSW | Switch to trigger irrigation after soil water potential has dropped below a minimum value | - |
| RAD | 1 degree in radians (180/PI) | radians |
| RADCAL | Current global radaition | Joule/(m² sec) |
| RADCPH | Photosynthetic active radiation under a clear sky | Joule/(m² sec) |
| RADFCN | Measured daily total global radiation table |  |
| RADIAT | Total incoming radiation | Joule/ ( $\mathrm{m}_{2}^{2} \mathrm{sec}$ ) |
| RADN | Radiation generating function | Joule/( $\mathrm{m}^{2} \mathrm{sec}$ ) |
| RADOPH | Photosynthetic active radiation under an overcast sky | Joule/ $\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| RAIN | Rainfall intensity | m/sec |
| RANGE | Range between average and minimum or maximum air temperature | degree ( ${ }^{\circ} \mathrm{C}$ ) |
| RANGES | Range between average and minimum or maximum soil temperature | degree ( ${ }^{\circ} \mathrm{C}$ ) |
| REFT | Reference or average air temperature | degree ( ${ }^{\circ} \mathrm{C}$ ) |
| REFTS | Reference or average soil temperature | degree ( ${ }^{\circ} \mathrm{C}$ ) |
| RELERR | CSMP statement - variable for integration control |  |
| RESL | Reserve level of carbohydrates in the plant | $\mathrm{kg} / \mathrm{m}^{2}$ |
| RESP | Total respiration of both root and shoot systems | $\mathrm{kg} /\left(\mathrm{m}_{2}^{2} \mathrm{sec}\right)$ |
| RESPRT | Total root respiration | $\mathrm{kg} /\left(\mathrm{m}_{2}^{2} \mathrm{sec}\right)$ |
| RESPSH | Total shoot respiration | $\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| RISE | Time of sunrise | hour |
| RISEI | Initial value of sunrise | hour |
| RK | Relative soil conductivity |  |
| RNF | Measured daily total rainfall table |  |
| RNFALL | Measured daily total rainfall | $\mathrm{m} / \mathrm{day}$ |
| ROOTDY | Root death rate | $\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| ROOTL | Total root length of living root tissue | $\mathrm{m} / \mathrm{m}$ |


| ROOTVL | Volume of living root tissue (by layer) | $\mathrm{m}^{3} / \mathrm{m}^{2}$ |
| :---: | :---: | :---: |
| R00TW | Total mass of living root tissue | $\mathrm{kg} / \mathrm{m}^{2}$ |
| ROOTWT | Mass of living root tissue (by layer) | $\mathrm{kg} / \mathrm{m}^{2}$ |
| RRL | Relative root length per layer | (dimensionless) |
| RRLL | Relative root mass per layer | gram/m |
| RRS | Radial resistance to root water uptake | sec |
| RSPFAC | Relative shoot maintenance respiration rate | kg/(kg sec) |
| RSRT | Root system resistance to water flow, total for each layer | sec m/m |
| RSSL | Soil resistance to water flow, total for each layer | $\mathrm{sec} \mathrm{m} / \mathrm{m}$ |
| RTDTH | Root death rate per layer | $\mathrm{m} / \mathrm{sec}$ |
| RTDWPC | Percentage dry matter in the roots | (dimensionless) |
| RTEX | Root extraction rate for soil moisture from each layer |  |
| RTGRES | Root growth respiration | $\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| RTGRO | Root growth rate per soil layer | $\mathrm{m} / \mathrm{sec}$ |
| RTMRES | Root maintenance respiration rate | $\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| RUN | Real number counting variable for printer output |  |
| RUNS | Integer number counting variable for printer output | - |
| SATCON | Saturated conductivity | $m * 10^{-2} /$ day |
| SCALE | Scale factor for vertical gradient plots |  |
| SHGRES | Shoot growth respiration rate | $\mathrm{kg} /\left(\mathrm{m}_{2}^{2} \mathrm{sec}\right)$ |
| SHMRES | Shoot maintenance respiration rate | $\mathrm{kg} /\left(\mathrm{m}_{2}^{2} \mathrm{sec}\right)$ |
| SHOOTD | Shoot death rate | $\mathrm{kg} /\left(\begin{array}{l} \\ 2\end{array} \mathrm{sec}\right)$ |
| SHOOTW | Mass of living shoot tissue | $\mathrm{kg} / \mathrm{m}^{2}$ |
| SIMDAY | Calendar day for input date | day |
| SIN | FORTRAN sine function | - |
| SLEVAP | Soil evaporation rate | $\mathrm{m} / \mathrm{sec}$ |
| SLLA | Sun lit leaf area index | $\mathrm{m}^{2} / \mathrm{m}^{2}$ |
| SMAX | Scaling factors for verticle gradient plotting |  |
| SMIN | Scaling factors for vertical gradient plotting | - |
| SNDC | Sine declination of the sun | (dimensionless) |
| SNHS | Sine of height of sun, but zero when sun below horizon | (dimensionless) |
| SNHSS | Sine of height of sun, also when negative | (dimensionless) |
| SNLT | Sine of latitude of experimental plot | (dimensionless) |
| SOLCHO | Soluble carbohydrate reserves (starch) in the plant | $\mathrm{kg} / \mathrm{m}^{2}$ |
| SQRT | FORTRAN function - square root | - |
| START | Beginning day for simulation run | day |
| STEMP | Temperature of the soil | degree ( ${ }^{\circ} \mathrm{C}$ ) |
| STEMW | Mass of the stem | kg |
| Storace | CSMP statement - allocation of memory locations |  |
| STWTR | Fraction of shoot dry matter, partitioned into the stem |  |
| SUMR | Sum of water removal by roots in all layers | m |
| SUMRD | Estimated root death rate for the whole plant | $\mathrm{m} /\left(\mathrm{m}_{2}^{2} \mathrm{sec}\right)$ |
| SUMRG | Estimated root grwoth rate for the whole plant | $\mathrm{m} /\left(\mathrm{m}_{2}^{2} \mathrm{sec}\right)$ |
| SUMRTD | Corrected root death rate for the whole plant | $\mathrm{m} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| SUMRTG | Corrected root growth rate for the whole plant | $\mathrm{m} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |


| SUNDCL | Direct visible radiation under a standard clear sky | Joule/(m² day) |
| :---: | :---: | :---: |
| SUNTB | Direct visible radiation under a standard clear sky table | - |
| SUTB | Suction table (volumetric water content versus soil suction, in meter ( $\mathrm{kPa} * 10$ ) ) | - |
| T | Real number representation for month |  |
| TCOM | Thickness of a soil layer (vertical direction) | $m$ |
| TEMP | Temperature of the air | degree ( ${ }^{\circ} \mathrm{C}$ ) |
| THETA | Volumetric water content of each soil layer |  |
| THTAIR | Minimum volumetric water content of top soil layer | $\mathrm{m}^{3} / \mathrm{m}^{3}$ |
| TIME | CSMP variable for simulation, initiating starting time | sec |
| TITLE | CSMP-statement |  |
| TMPFCR | Biological $Q_{10}$-value - temperature factor for the roots | (dimensionless) |
| TMPFCS | Biological $Q_{10}$-value - temperature factor for the shoot | (dimensionless) |
| TOPGRO | Total growth of the shoot system | $\mathrm{kg} /\left(\mathrm{m}_{2}^{2} \mathrm{sec}\right)$ |
| TOTRG | Total growth of the root system | $\mathrm{kg} /\left(\mathrm{m}^{2} \mathrm{sec}\right)$ |
| TRANSP | Transpiration loss | $\mathrm{m} / \mathrm{sec}$ |
| TRNTBL | Transpiration table | - |
| TT | Integer number representation for month | - |
| UARS | Unit axial resistance per unit root surface | $\mathrm{sec} \mathrm{m} / \mathrm{m}$ |
| UPDATE | Name of FORTRAN program generated to update integration | - |
| URRS | Unit radial resistance per unit root surface | s |
| VOLW | Voume of water in each compartment | /m |
| W | Water potential difference for extension of new roots in second soil layer | m (kPa*10) |
| WATER | Measured daily total rainfall (constant over a day) | m/day |
| WATRST | Water stress in plant tissue (relative 0-1 factor, based on canopy water potential) | (dimensionless) |
| WAVE | ```Macro for the computation of temperature along sine profile``` |  |
| X | Water potential difference for branching rate of new roots | m (kPa*10) |
| XOVC | Auxiliary variable to calculate photosynthesis (fraction overcast) | (dimensionless) |
| XS | Auxiliary variable to calculate photosynthesis | (dimensionless) |
| XSH | Auxiliary variable to calculate photosynthesis (fraction sunshine) | (dimensionless) |
| XX | Water potential difference for extension of new roots | $\mathrm{m}(\mathrm{kPa} * 10)$ |
| Y | Vertical gradient plotting variable | - |
| YY | Runner for vertical gradient plotting | - |

ZHOLD CSMP function - storing integration value
ZLAM Z(lambda), parameter to compute soil hydraulic conductivity
(dimensionless)
ZYX Debug statement argument
ZYY Debug statement argument
ZZZ Debug statement argument


[^0]:    ${ }^{1}$ Part of a dissertation submitted by the senior author in partial fulfillment of the requirements for the Ph.D. degree.
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    ${ }^{3}$ Mention of a trade name is solely for the convenience of the reader and does not imply endorsement of that product to the exclusion of others by the U.S. Department of Agriculture or by Auburn University or its employees.

[^1]:    1Units are given for information only and are not generated during the actual simulation run.

